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Direct Numerical Simulation of Turbulent Lean Premixed H₂/Air Flames at Elevated Pressure

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Contents

- Background
- Numerical method and computational cases
- Results and discussion
- Conclusions

1 Background

- ❑ There has been considerable interest in lean premixed H_2 /air combustion which reduces peak temperature and consequently thermal NO_x emission. No significant changes to current combustion facilities.
- ❑ It is hard to get detailed information of elevated pressure combustion in experiments. Most of DNS studies of flame structure and propagation are carried out at atmospheric pressure.
- ❑ 3D-DNS studies with detailed chemistry at elevated pressures are few and far inbetween. Understanding of combustion characteristics at elevated pressure is insufficient.

2 Objectives

- Study the instantaneous flame structure at different pressure levels
- Study the flame instability at different pressure levels

3 Numerical Approach DNS

- Navier-Stokes equations and chemical species transport equations are solved with six-order compact finite difference schemes for spatial discretization and low-storage third-order Runge-Kutta time advancing scheme is used for the time advancement.
- The Navier-Stokes Characteristics Boundary Conditions (NSCBS) are applied at the inlet / outlet and periodic boundary conditions are imposed in the spanwise and lateral directions.

3 Numerical Approach DNS

- Turbulence was generated in a periodic box, which was then fed into the inlet plane of the main simulation.
- A one-dimensional (1D) laminar flame was generated using detailed chemistry and detailed transport properties to initialize the three-dimensional turbulent flame simulation.
- Chemical mechanism is from Li et al.[1], involving 9 species and 21 reactions.

[1]Li, Juan, et al. "An updated comprehensive kinetic model of hydrogen combustion." *International journal of chemical kinetics* 36.10 (2004): 566-575.

4 Computational Cases

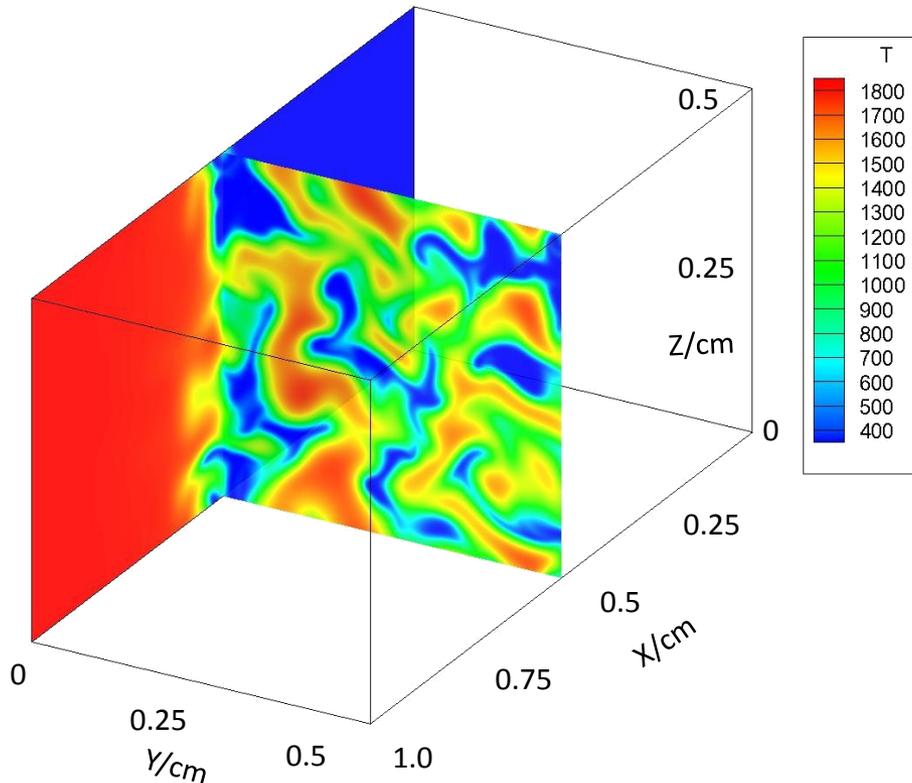


Fig.1 A schematic of computational domain .

Table 1 Key parameters in computational cases

Case	P=1atm	P=2atm	P=5atm
Equivalence ratio	0.6	0.6	0.6
S_L (cm/s)	88.5	69.9	47.9
δ_L (cm)	3.85E-02	1.9E-0.2	8.24E-0.3
u' (cm/s)	1138	1138	1138
l (cm)	0.0628	0.0628	0.0628
Grid resolution (μm)	10.01	9.77	9.77
$\Delta x/\eta$	0.156	0.309	0.768
Re_T	21	54	181

*Note:

S_L - laminar flame speed

δ_L - laminar flame thickness

u' – Root-mean-square turbulent fluctuation velocity

l - Integral length scale

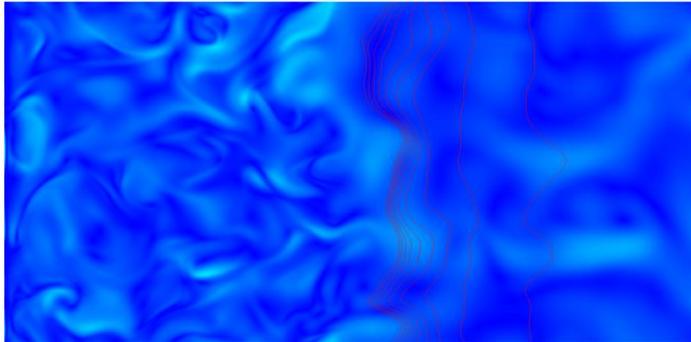
Turbulent Reynolds number $Re_T = \frac{u'l}{\delta_L S_L}$

Kolmogorov length scale $\eta = l \cdot Re_T^{-3/4}$

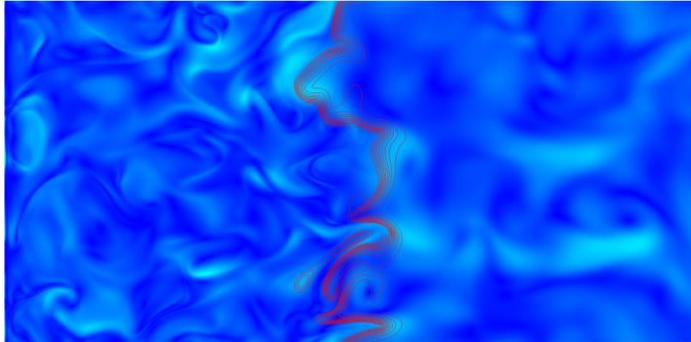
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Instantaneous Flame Structure

P=1atm



P=2atm



P=5atm

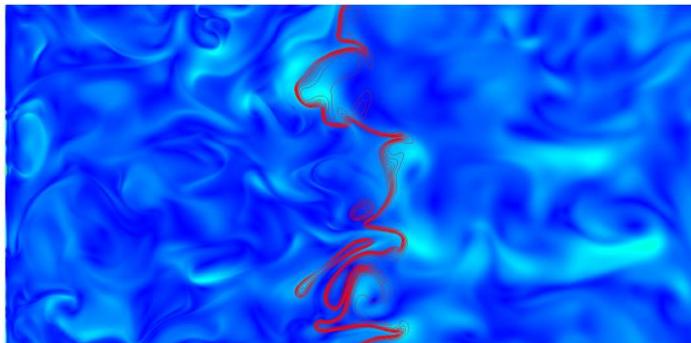


Fig.2 2D snapshots of vorticity field (red lines for progress variable $c=0.1-0.9$)

Non-dimensional progress variable
$$c = \frac{T - T_u}{T_b - T_u}$$

- The three flames are considered within the Thin Reaction zone.
- The flame zone is considered to be bounded by $c=0.1$ and $c=0.9$. Small scale turbulent eddies could not enter the reaction zone.
- When $P= 5\text{atm}$, the reaction zone is much thinner than that under atmospheric pressure.

5

Instantaneous Flame Structure

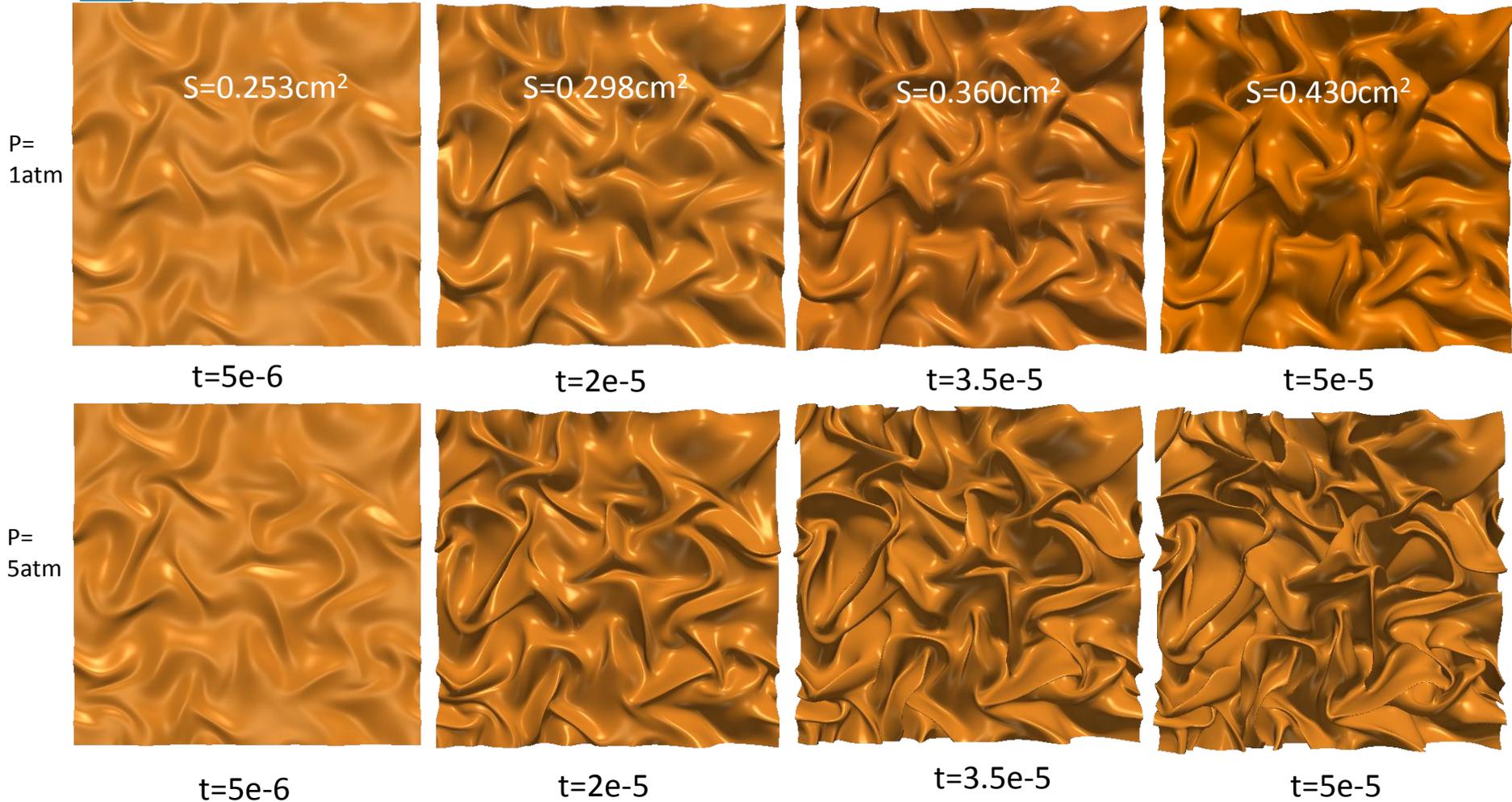


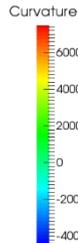
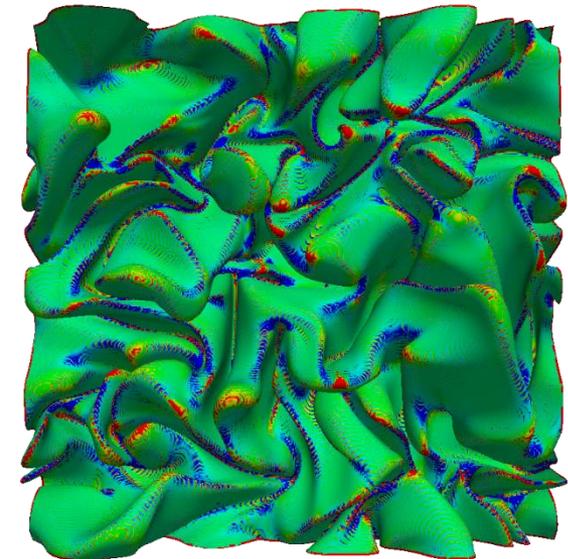
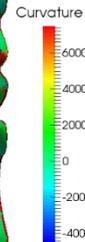
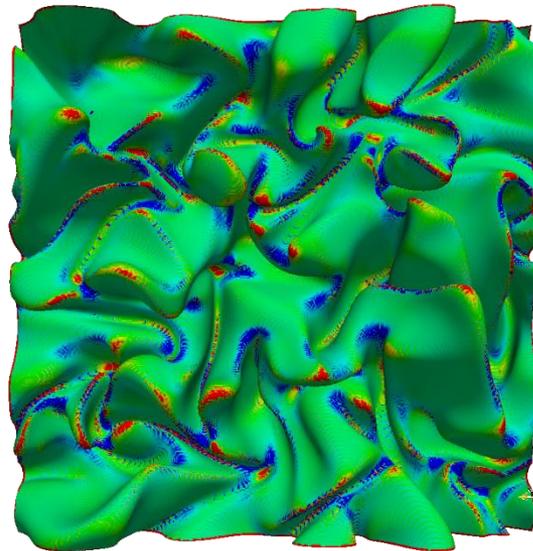
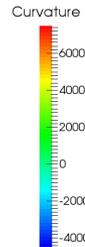
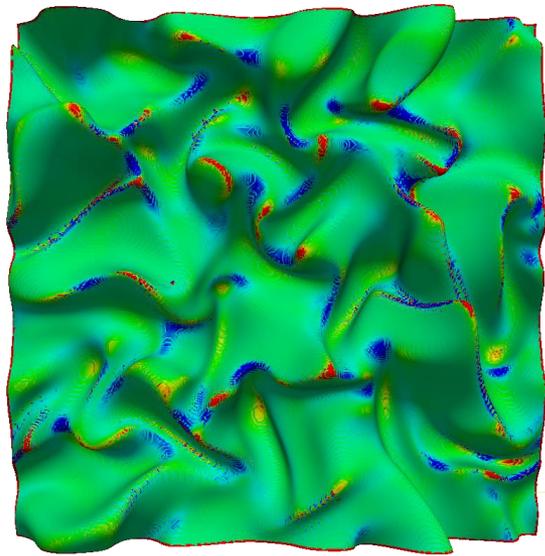
Fig.3 sequences of flame propagation(iso-surface $c=0.5$)

5 Instantaneous Flame Structure

$S=0.430\text{cm}^2$

$S=0.635\text{cm}^2$

$S=0.908\text{cm}^2$



P=1atm

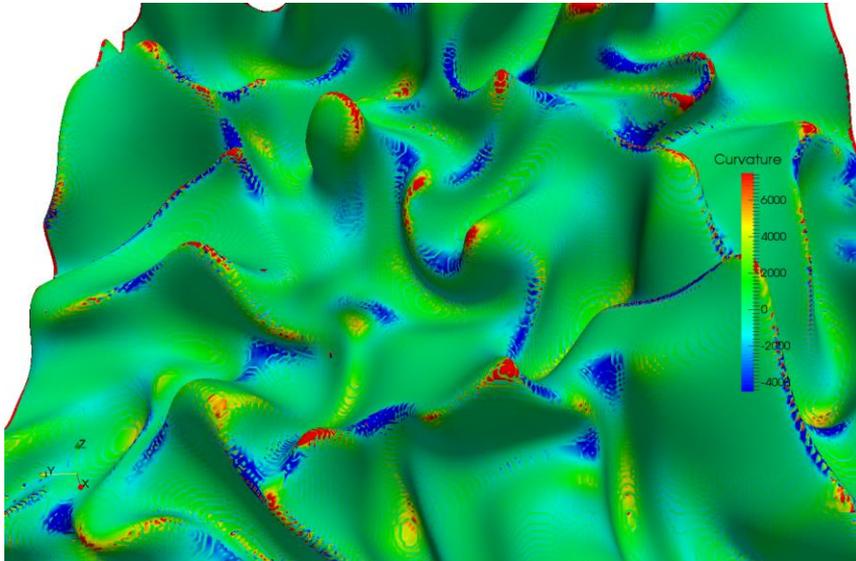
P=2atm

P=5atm

Fig.4 Iso-surfaces of flame front, coloured by curvature ($t=5e-5$, $c=0.5$)

5 Instantaneous Flame Structure

P=1atm



P=5atm

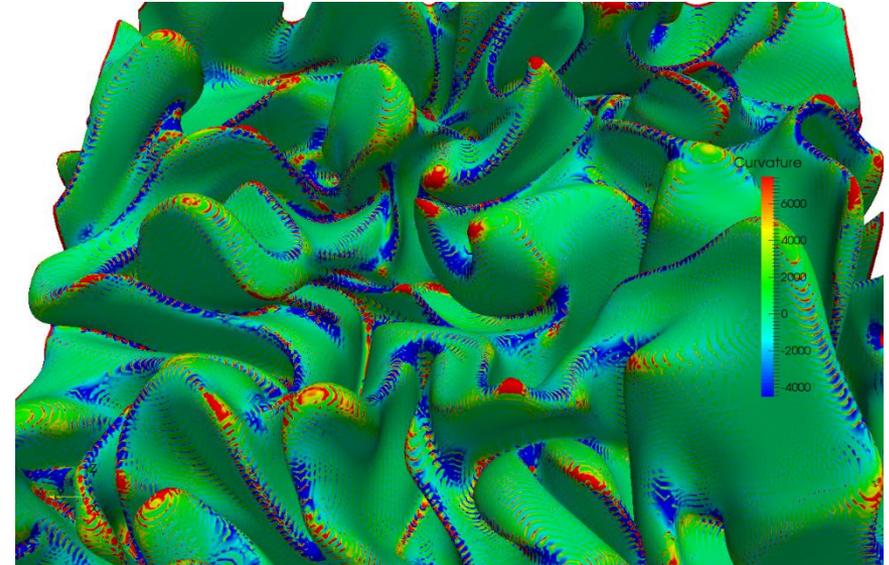
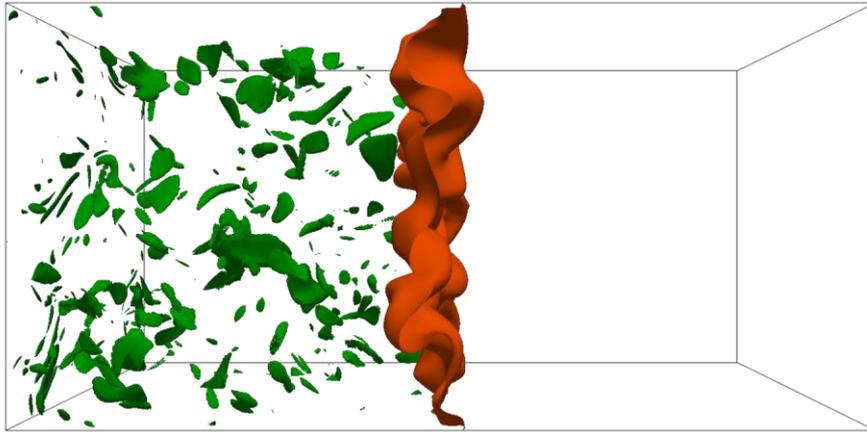


Fig.5 Details of iso-surfaces

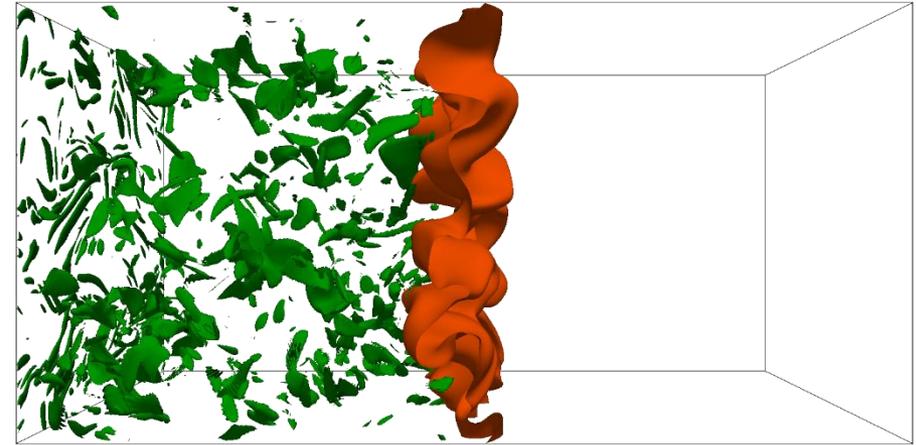
- The three cases are initialized with same turbulence field. The flame surface is wrinkled immediately after initiation of propagation.
- The flames under higher pressure exhibit more small scales structures and as a result flame wrinkling is getting stronger. It is associated with flame instabilities and turbulent levels at elevated pressure.

7

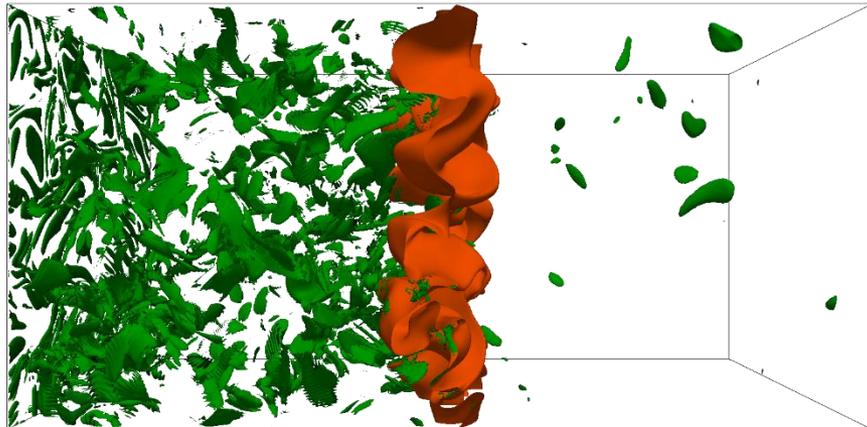
Influence of turbulence



P=1atm



P=2atm



P=5atm

Fig.6 Instantaneous vortex structures at different pressures (red surface $c=0.5$)

$$Q_criterion \quad Q_- = \frac{1}{2} \frac{\partial u_i}{\partial x_j} \frac{\partial u_j}{\partial x_i}$$

- Under high pressure, the vortex structures tend to be complex and unsteady, which contributes to more small flame cells

7

Dissusion

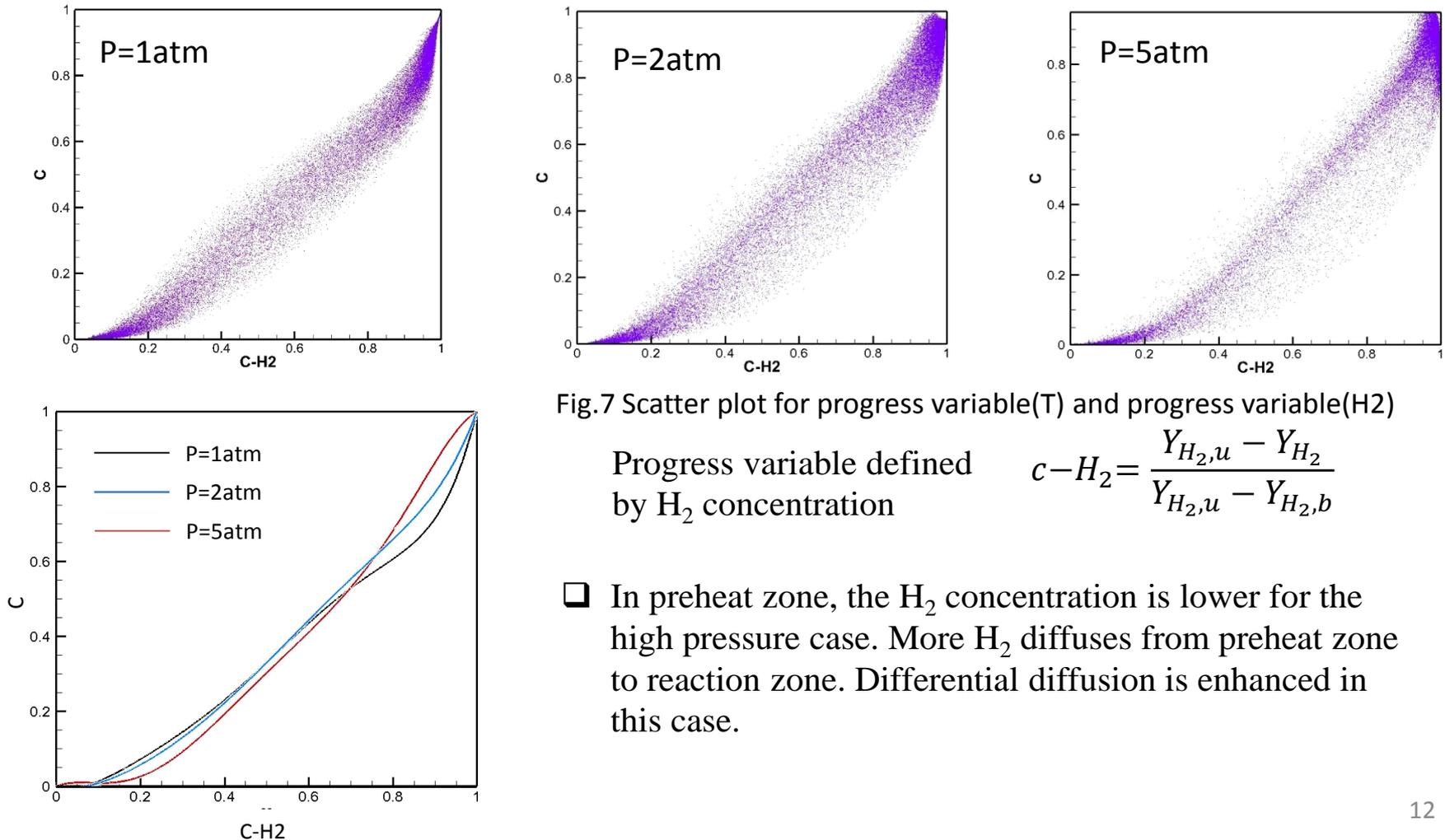


Fig.7 Scatter plot for progress variable(T) and progress variable(H2)

Progress variable defined by H₂ concentration

$$c-H_2 = \frac{Y_{H_2,u} - Y_{H_2}}{Y_{H_2,u} - Y_{H_2,b}}$$

- In preheat zone, the H₂ concentration is lower for the high pressure case. More H₂ diffuses from preheat zone to reaction zone. Differential diffusion is enhanced in this case.

7

Conclusions and plans

- The reaction zone is seriously narrowed at elevated pressure for turbulent lean premixed H₂/Air combustion.
- Under high pressure, there are more small flame structures than low pressure. Flame wrinkling tends to be stronger.
- Under high pressure, differential diffusion is enhanced and vortex structures tend to be complex and unsteady.
- In the future, we will focus on: the influence of differential diffusion and turbulent levels on flame properties at elevated pressure.

Acknowledgement

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Thank you!