

High fidelity simulations of turbulent combustion applications using the parallel multiphysics code Alya

E. Illana¹, O. Lehmkuhl², D. Mira², S. Gövert³, M. Vázquez², G. Houzeaux², X. Jiang¹, J.B.W. Kok³

¹Queen Mary University of London, London, United Kingdom ²Barcelona Supercomputing Center, Barcelona, Spain ³University of Twente, Enschede, The Netherlands









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Simulations of turbulent combustion, which involves complex coupled multi-physic phenomena, can play an important role in the development of combustors

- Optimization of combustor designs towards systems with:

- Increased thermal efficiency
- Low emissions level
- o Fuel flexibility
- High acoustic stability
- Minimize the cost:
 - Reduce the amount of experimental testing
 - Better insight of the flow field and flame dynamics



- 1. Computational framework
 - Alya
- 2. Modelling approach
 - Governing equations
 - Thermochemical database
- 3. Test cases
 - Sandia flame
 - PRECCINSTA
- 4. Conclusions and future work
- 5. Acknowledgements



Alya is in the PRACE benchmark suite

Available online at www.prace-ri.eu a final list of 12 codes to form the initial version of UEABS, w PRACE Partnership for Advanced Computing in Europe QCD **Particle Physics:** NAMD, GROMACS Classical MD: Quantum Espresso, CP2K, GPAW **Ouantum MD:** Code Saturie, ALYA CFD: NEMO, SPECFEM5D Earth Sciences: Selection of a Unified European Application Benchmark Suite Plasma Physics: GENE J. Mark Bull^a*, Andrew Emerson^b GADGET Astrophysics: 'EPCC, University of Edinburgh, King's Buildings, Mayfield Road, Edinburgh EH9 3JZ, UK CINECA, via Magnanelli 6/3, 40033 Casalecchio di Reno, Bologna, Ita Lindgren - Cray XE6 Jugene - Blue Gene/P Curie - BullX Blue Waters - Cray XE6 Sweden France Germany USA Average # elements per CPU 183k 64k 365k 91k 45k 730k 92k 200k 50k 25k 129k 42k 24000 100000 14000 16000 Ideal Ideal Ideal Ideal Blue Waters ----Lindgren -----...... ---Jugene Curie 12000 14000 20000 80000 10000 12000 16000 60000 8000 10000 12000 6000 8000 40000 8000 4000 6000 20000 4000 2000 4000 0 1536 6144 12288 2048 8192 16384 2816 11264 22528 32768 65536 100000 Number of CPU's Number of CPU's Number of CPU's Number of CPU's







BIOMASS FOR ENERGY – Governing equations



Continuity:
$$\frac{\partial \bar{\rho}}{\partial t} + \nabla \cdot (\bar{\rho}\tilde{u}) = 0$$
burntMomentum: $\frac{\partial (\bar{\rho}\tilde{u})}{\partial t} + \nabla \cdot (\bar{\rho}\tilde{u}\tilde{u}) = -\nabla \bar{p} + \nabla \cdot \tau$ unburntEnergy: $\frac{\partial (\bar{\rho}\tilde{h})}{\partial t} + \nabla \cdot (\bar{\rho}\tilde{u}\tilde{h}) = \nabla \cdot \left[\left(\frac{\bar{\lambda}}{\bar{c}p} + \frac{\mu_t}{Sc_t} \right) \nabla \tilde{h} \right]$ $\nabla \tilde{h}$ Progress variable: $\frac{\partial (\bar{\rho}\tilde{c})}{\partial t} + \nabla \cdot (\bar{\rho}\tilde{u}\tilde{c}) = \nabla \cdot \left[\left(\frac{\bar{\lambda}}{\bar{c}p} + \frac{\mu_t}{Sc_t} \right) \nabla \tilde{c} \right] + \tilde{\omega}_c$

Progress variable variance:

$$\frac{\partial(\bar{\rho}\widetilde{c_{v}^{2}})}{\partial t} + \nabla \cdot (\bar{\rho}\widetilde{u}\widetilde{c_{v}^{2}}) = \nabla \cdot \left[\left(\frac{\bar{\lambda}}{\bar{c_{p}}} + \frac{\mu_{t}}{Sc_{t}} \right) \nabla \widetilde{c_{v}^{2}} \right] + 2\left(\widetilde{c\ \omega_{c}} - \widetilde{\omega_{c}}\ \widetilde{c} \right) + 2\bar{\rho}\frac{\mu_{t}}{Sc_{t}} \left(|\nabla\widetilde{c}|^{2} - \frac{\widetilde{c_{v}^{2}}}{\Delta^{2}} \right) + 2\bar{\rho}\frac{\mu_{t}}{Sc_{t}} \left(|\nabla\widetilde{c}|^{2} - \frac{\widetilde{c_{v}}}{\Delta^{2}} \right) + 2\bar{\rho}\frac{\mu_{t}}{Sc_{t}} \left(|\nabla\widetilde{c}|^{2} - \frac{$$

$$\frac{\partial(\bar{\rho}\tilde{Z})}{\partial t} + \nabla \cdot (\bar{\rho}\tilde{u}\tilde{Z}) = \nabla \cdot \left[\left(\frac{\bar{\lambda}}{\bar{c_p}} + \frac{\mu_t}{Sc_t} \right) \nabla \tilde{Z} \right]$$

Mixture fraction variance:

$$\frac{\partial(\bar{\rho}\widetilde{Z_{\nu}})}{\partial t} + \nabla \cdot (\bar{\rho}\widetilde{u}\widetilde{Z_{\nu}}) = \nabla \cdot \left[\left(\frac{\bar{\lambda}}{\bar{c_{p}}} + \frac{\mu_{t}}{Sc_{t}} \right) \nabla \widetilde{Z_{\nu}} \right] + 2 \frac{\mu_{t}}{Sc_{t}} \left(\left| \nabla \widetilde{Z} \right|^{2} - \frac{\widetilde{Z_{\nu}^{2}}}{\Delta^{2}} \right)$$

WP5 BIOMASS FOR ENERGY – Premixed flamelets





- Enthalpy and mixture fraction (Z) are constant along the flame
- Solution are calculated at Z values within the flammability limits
- Space variable changed to reaction progress variable:

$$c = \frac{\sum a_k (Y_k - Y_{k,in})}{\sum a_k (Y_{k,out} - Y_{k,in})}$$

- Presumed Beta-PDF for the calculation of the mean Favre-averaged quantities
- RPV source term, transport properties and NASA polynomial coefficients are tabulated

Source term and properties are computed tabulated for several non-dimensional enthalpy values

$$i = \frac{h - h_{min}}{h_{max} - h_{min}}$$



- *h_{max}* is defined from adiabatic conditions
- *h_{min}* is determined from the value at which the flame speed is almost negligible
- Source term is zero if $h < h_{min}$
- Effect of enthalpy variance is neglected



BIOMASS FOR ENERGY – Sandia D flame





Mesh 3

50M

25% CH₄, 75% Dry Air

BIOMASS FOR ENERGY – Sandia D flame







Fuel	<i>ṁ_{air}</i> (g∕s)	<i>ṁ_f</i> (g/s)
CH_4	12.2366	0.5983
75% CH ₄ 25% CO ₂	12.2366	1.1468
50% CH ₄ 50% CO ₂	12.2366	2.2437
50% CH ₄ 40% CO ₂ 10% N ₂	12.2366	2.1241

































BIOMASS FOR ENERGY – Averaged temperature fields





BIOMASS FOR ENERGY – Averaged temperature lines





BIOMASS FOR ENERGY – Averaged velocity fields



 U_x (m/s)

90.

60

30

0

-30.





BIOMASS FOR ENERGY – Averaged velocity lines



BIOMASS FOR ENERGY – Averaged CO fields





BIOMASS FOR ENERGY – Averaged CO lines



BIOMASS FOR ENERGY – Averaged NO fields





BIOMASS FOR ENERGY – Averaged NO lines





BIOMASS FOR ENERGY – Axial line







- Alya has a high potential for performing **large-scale simulations** of practical combustion systems.
- The turbulent combustion model uses **tabulated source terms and properties** that depend on the progress variable, the mixture fraction, their variances and a non-dimensional enthalpy
- Model gives reasonable results when compared to experimental data
- Despite the difference in flame temperature, the velocity fields are not highly affected by the fuel type

- Simulations with a non-premixed setup should introduce further velocity discrepancies between the cases
- Combination of premixed tables with diffusion tables can potentially improve the accuracy of the results

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HP

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