



# **Response of heat release to equivalence ratio variations in high Karlovitz premixed H<sub>2</sub>/air flames at 20 atm: a DNS study**

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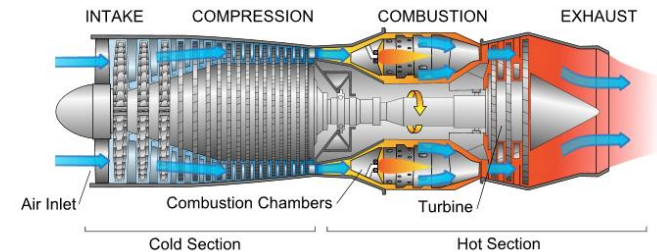
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## Outline

- ☐ Background
- ☐ Numerical method and computational cases
- ☐ Results and discussion
- ☐ Conclusions and future work

# 1 Background



- ❑ Lean premixed combustion has wide-ranging applications in industrial devices with the advantage of low NO<sub>x</sub> emission. In modern gas turbines, typical equivalence ratios at base load are in the range 0.45-0.6 [1].
- ❑ Turbulent flames in gas turbines are characterised by intense turbulence intensity and high pressure.
- ❑ Turbulent lean premixed flames are susceptible to equivalence ratio oscillation, which is one of the most significant mechanisms contributing to combustion instabilities.
- ❑ Objectives: To study the characteristics of lean H<sub>2</sub>/air flames with various equivalence ratios under conditions relevant to gas turbines (High Ka, High P) by three-dimensional direct numerical simulations .

## 2 Direct numerical simulation

- ❑ DNS code: PENCIL CODE[1]
- ❑ Spatial discretization — six-order compact finite difference schemes
- ❑ Time advancement — low-storage third-order Runge-Kutta (RK3-2N)
- ❑ Chemistry calculation — Livermore Solver for ODE (LSODE)
- ❑  $\text{H}_2/\text{O}_2$  chemical mechanism developed by Li et al. (2004)

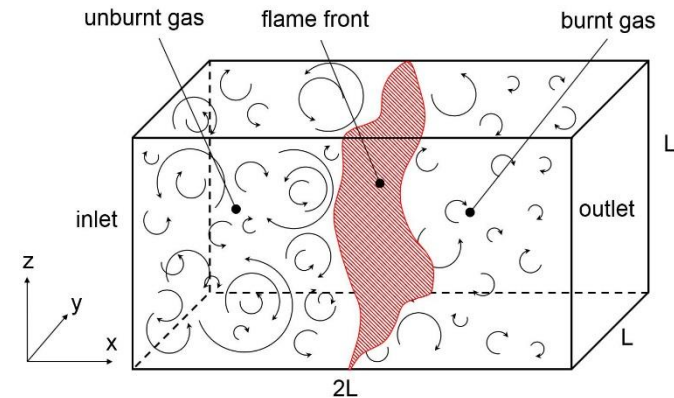


Fig. 1 Schematic of the computational domain .

### Boundary conditions:

- ❑ Cross-flow direction: periodic boundary conditions
- ❑ Inlet/outlet: NSCBS

[1] Babkovskaia N, Haugen NEL, Brandenburg A. A high-order public domain code for direct numerical simulations of turbulent combustion. J Comput Phys 2011;230(1):1-12.

### 3 Computational Cases

Pressure=20atm

**Table 1. Simulation parameters.**

Case	A	B	C
$\phi$	<b>0.4</b>	<b>0.5</b>	<b>0.6</b>
$S_L$ (cm/s)	1.66	6.81	21.16
$\delta_L$ (cm)	2.54E-02	8.3E-03	3.3E-03
$u'$ (cm/s)	177	664	1941
$\nu$ (cm <sup>2</sup> /s)	9.05E-03	9.34E-03	9.62E-03
$l_t$ (cm)	2.54E-02	8.3E-03	3.3E-03
$\Delta x$ ( $\mu$ m)	4.96	3.24	1.29
Re	497	590	666
Ka	<b>2376</b>	<b>2373</b>	<b>2368</b>

Turbulent Reynolds number  $Re = u' l_t / \nu$

Karlovitz number  $Ka = (u'^3 / \nu l_t)^{1/2} / (S_L / \delta_L)$

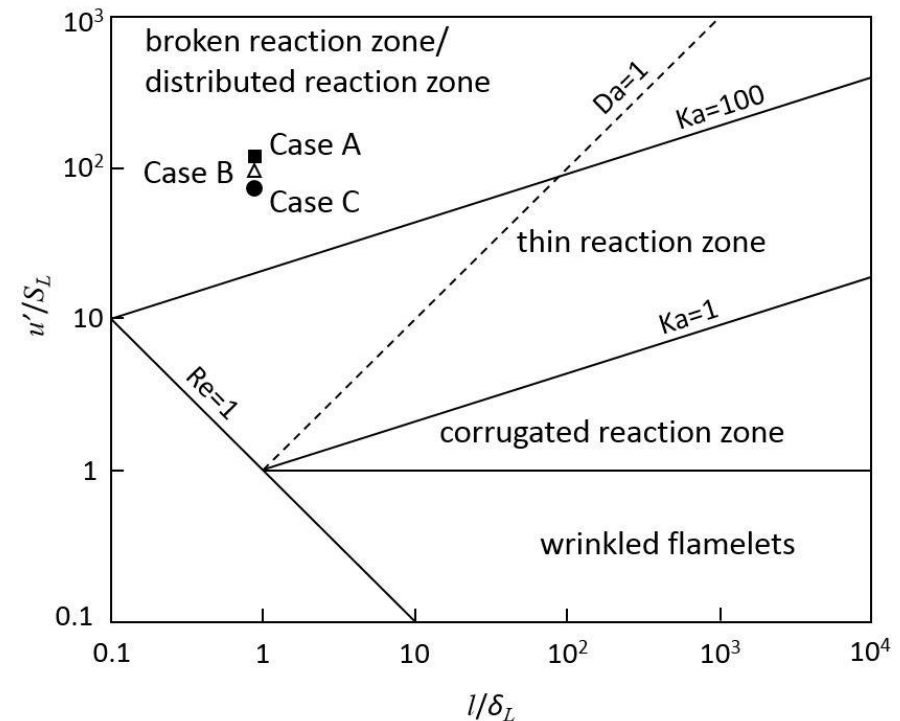


Fig. 2 Turbulent combustion regime diagram

#### Initial condition:

- Pre-generated 1D flame + turbulence
- 26 grids across the flame thickness
- Time step is determined by CFL condition:  $1e-10 \sim 2.5e-9$

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## Results: 1D laminar flame

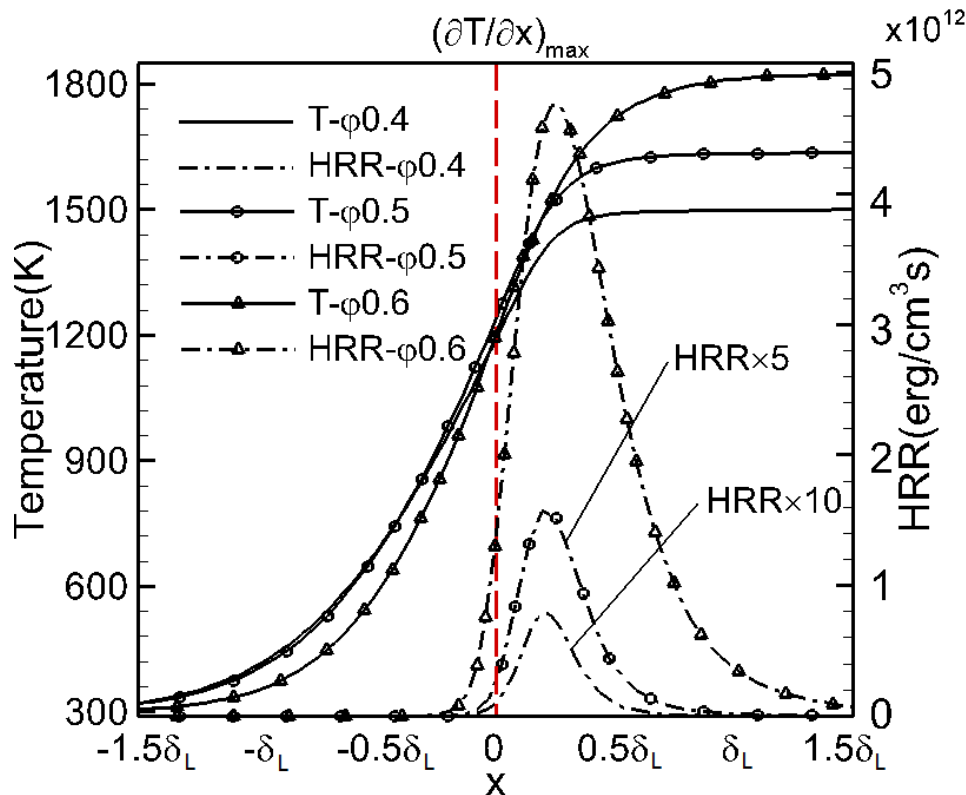


Fig.3 Laminar flame structures

- HRR is significantly increased when the equivalence ratio increases
- The burnt gas temperature increases from 1530 K to 1836 K
- The equivalence ratio increases, the reaction zone is obviously broadened.
- The scaled temperature gradient is larger under higher equivalence ratio

## 4 Results: flame structures

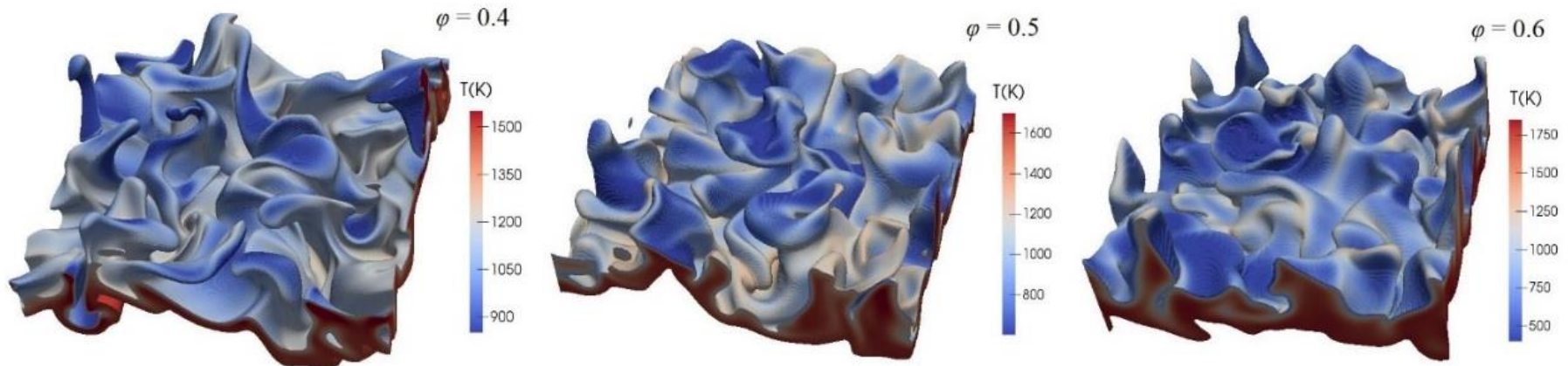
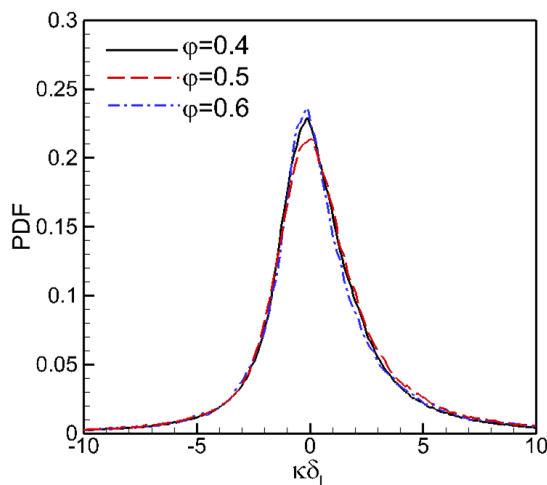


Fig. 4 Reaction zone structures at different equivalence ratios.



- ❑ the flame fronts are seriously wrinkled and stretched by turbulences
- ❑ Characterized by the same Ka, the flame front structures of the three flames are quite similar.
- ❑ The Pdf of mean curvatures of flame fronts are consistent.

Fig.5 PDFs of mean curvatures of flame fronts

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## Results: flame structures

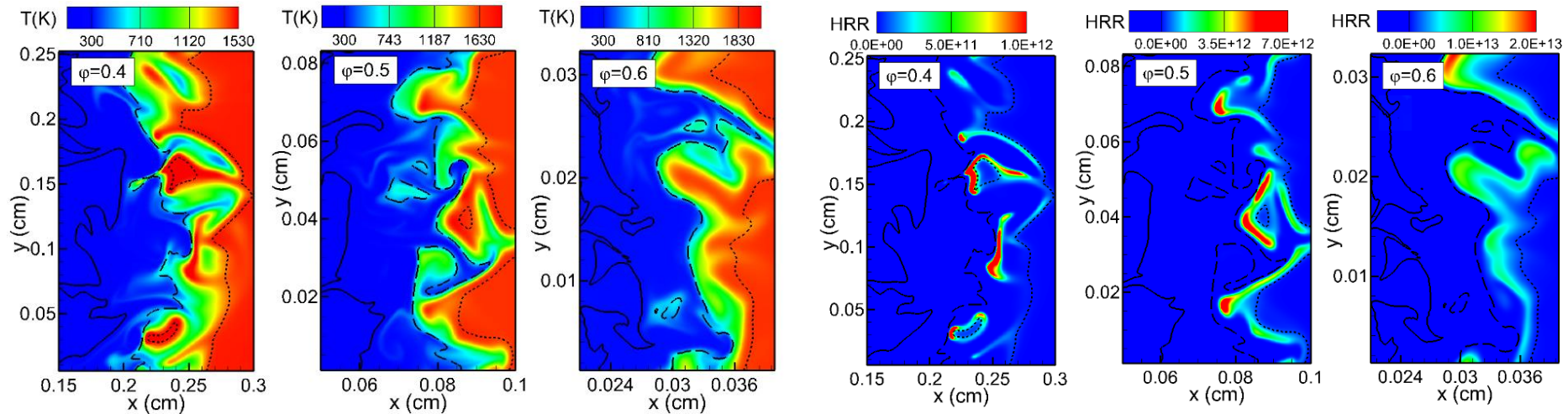
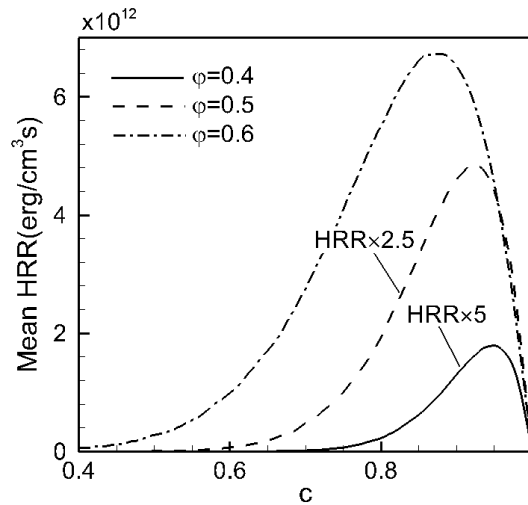


Fig. 6 2D snapshot of reaction zone structures at different equivalence ratios. The solid, dashed and dotted black lines correspond to  $c = 0.01$ ,  $0.5$  and  $0.99$ , respectively.

- ❑ The majority of heat release happens in region  $0.5 < c < 0.99$
- ❑ the thickness of high-HRR regions is obviously increased, and the gradient is correspondingly decreased. In flame C, the high-HRR regions almost fill up the zone  $0.5 < c < 0.99$ , whereas there are only narrow strips in flame A.



## 4 Results: flame mean statistics



- the heat release of turbulent flames is enhanced, and the reaction layer is relatively broadened under high equivalence ratio.
- the extent of enhancement is reduced at high equivalence ratio.
- obvious heat release is observed from  $c = 0.4$  for case  $\varphi = 0.6$ , while it happens after  $c = 0.7$  for case  $\varphi = 0.4$ .

Fig.7 Mean heat release versus progress variable for turbulent flames

Table 2 Characteristic parameters of reaction zones of laminar and turbulent flames

Case	$\text{HRR}_{\text{max\_1D}}$ (erg/cm <sup>3</sup> s)	Mean $\text{HRR}_{\text{max\_3D}}$ (erg/cm <sup>3</sup> s)	$\delta_{\text{f\_1D}}$	$\delta_{\text{f\_3D}}$
A	7.90E10	3.69E11	0.54 $\delta_{\text{L}}$	1.25 $\delta_{\text{L}}$
B	7.87E11	1.95E12	0.65 $\delta_{\text{L}}$	1.63 $\delta_{\text{L}}$
C	4.68E12	6.73E12	$\delta_{\text{L}}$	1.86 $\delta_{\text{L}}$

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## Results: local equivalence ratio $\varphi_L = \frac{Y_H / (2 \cdot W_H)}{Y_O / W_O}$

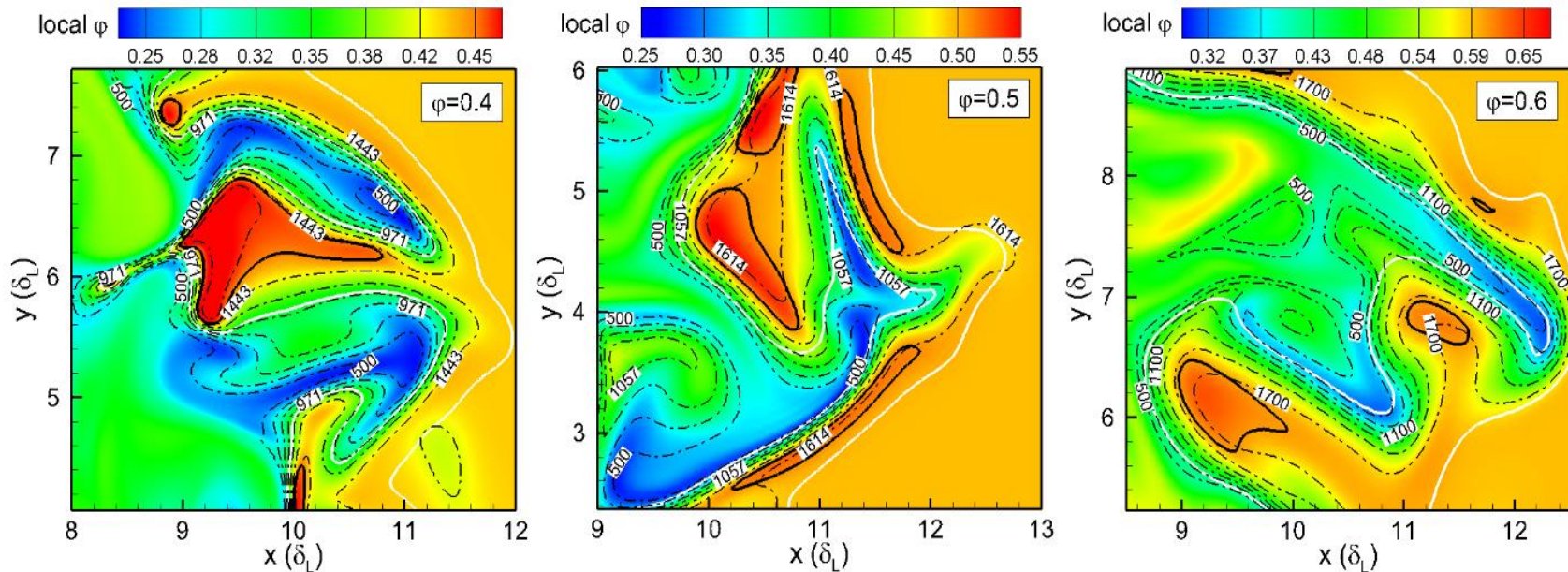
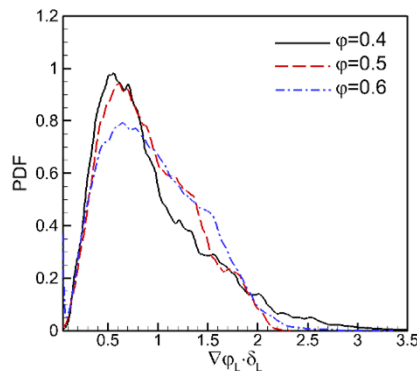


Fig.8 Two-dimensional slices of the reaction zone coloured by local equivalence ratio



- ☐  $\varphi_L$  is significantly lower than the fresh gas  $\varphi$  in the upstream near the reaction layer
- ☐  $\varphi_L$  trenches and plateaus are situated on two sides of the left boundary of reaction zone
- ☐ With increasing equivalence ratio, the difference of gradients is reduced

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## Results: local equivalence ratio

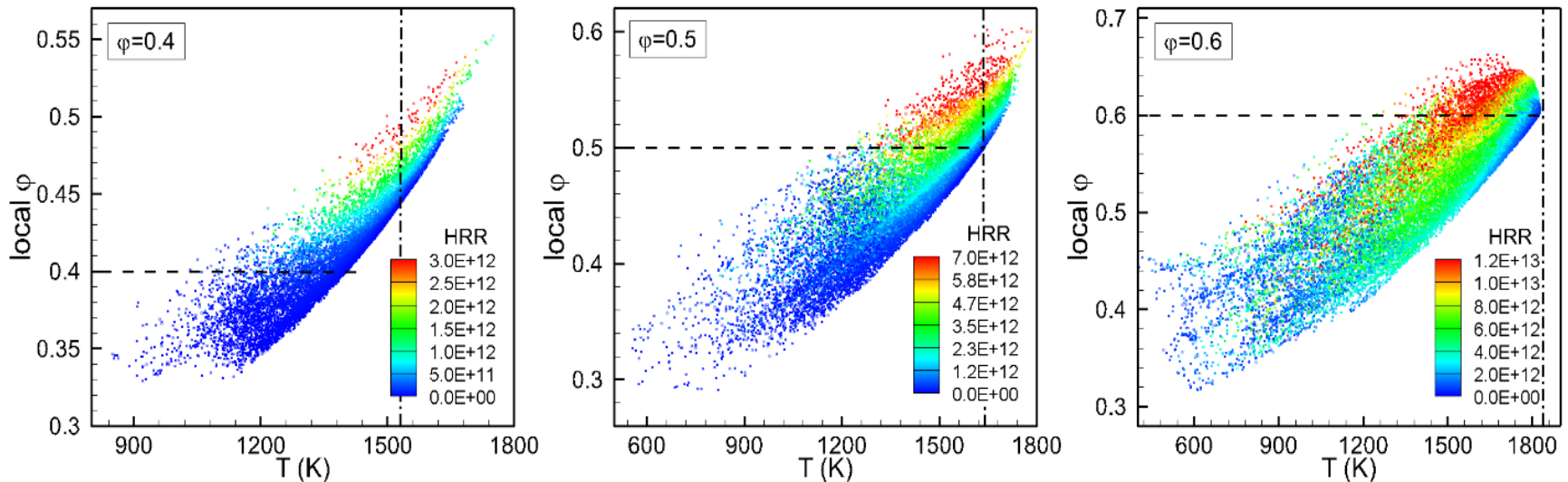


Fig.10 Scatter plots of local temperature and local equivalence ratio in the reaction zone.

- ☐ The scatter distribution shows a positive correlation between  $\phi_L$  and temperature
- ☐ Hot spots with temperature higher than the adiabatic temperature are observed under ultra-lean conditions

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## Results: HRR marker

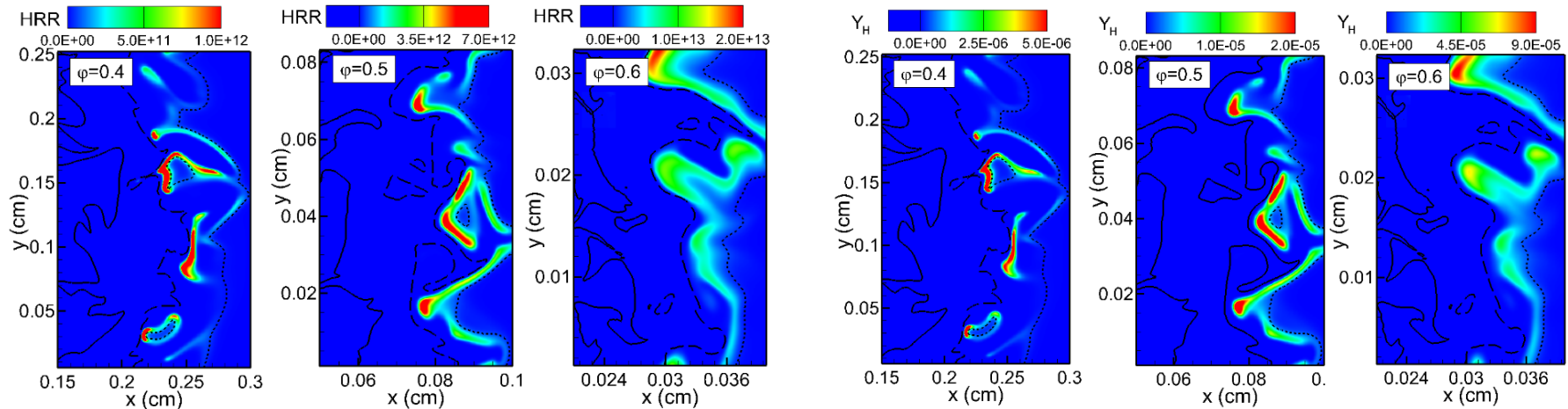


Fig.11 Two-dimensional snapshots of regions around reaction zones showing heat release rates, and H mass fraction for the cases with equivalence ratios 0.4, 0.5 and 0.6. The solid, dashed and dotted black lines correspond to  $c = 0.01$ ,  $0.5$  and  $0.99$ , respectively.

- In experimental studies, the heat release regions cannot be directly measured
- the contour of H mass fraction agrees well with the contour of HRR
- H could be used as a reliable HRR marker in high-pressure lean flames with varying equivalence ratios?

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## Results: HRR marker

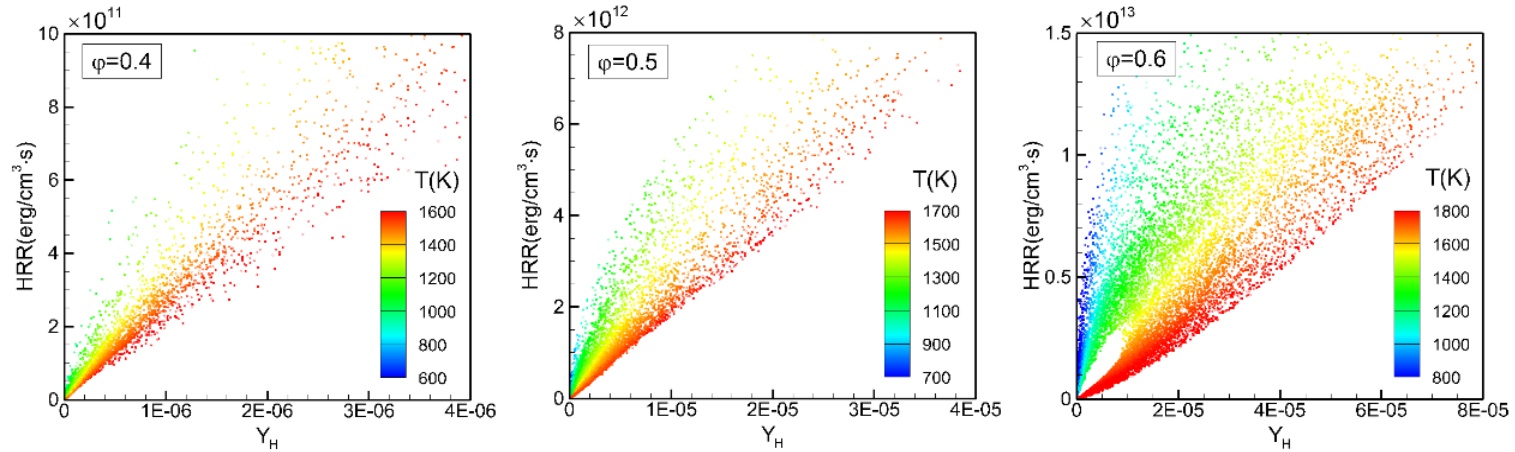
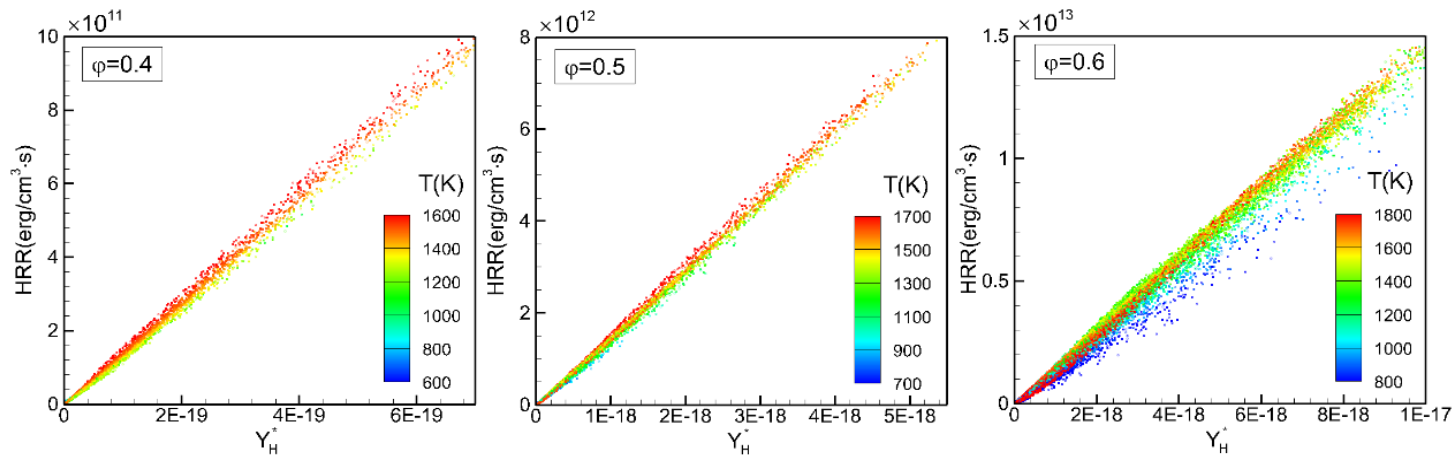


Fig.12 Scatter plots of H mass fraction and heat release



$$Y_H^* = Y_H / T^n$$

$$n = 4$$

$$HRR = \alpha Y_H^* / T^4$$

$$\alpha = 1.43e30 - 1.5e30$$

Fig.13 Scatter plots of scaled H mass fraction and heat release

## 6

## Conclusions

- ❑ The characteristics of heat release under various equivalence ratios are investigated by three-dimensional direct numerical simulations of lean  $\text{H}_2$ /air flames under conditions relevant to gas turbines.
- ❑ Under different lean conditions ( $\varphi = 0.4, 0.5, 0.6$ ), the turbulent flame fronts show similar topological structures for the three cases under the same Karlovitz number.
- ❑ Trenches of local equivalence ratio  $\varphi_L$  are located at concave structures outside the reaction zone, while  $\varphi_L$  plateaus are situated at convex structures inside the reaction zone.
- ❑ With increasing equivalence ratio, the difference of gradients in convex and concave regions is reducing.
- ❑  $\varphi_L$  is found to be significantly higher than mixture  $\varphi$  under ultra-lean conditions, resulting in hot spots in the reaction zone.
- ❑ Radical H could be used as a perfect HRR marker when it is scaled by temperature.

Thank you!

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