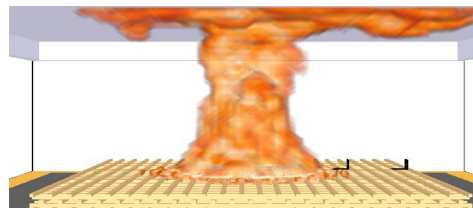


# “Scaling-up” fire spread on wood cribs using CFD

UKCTRF Annual conference  
13 September 2022



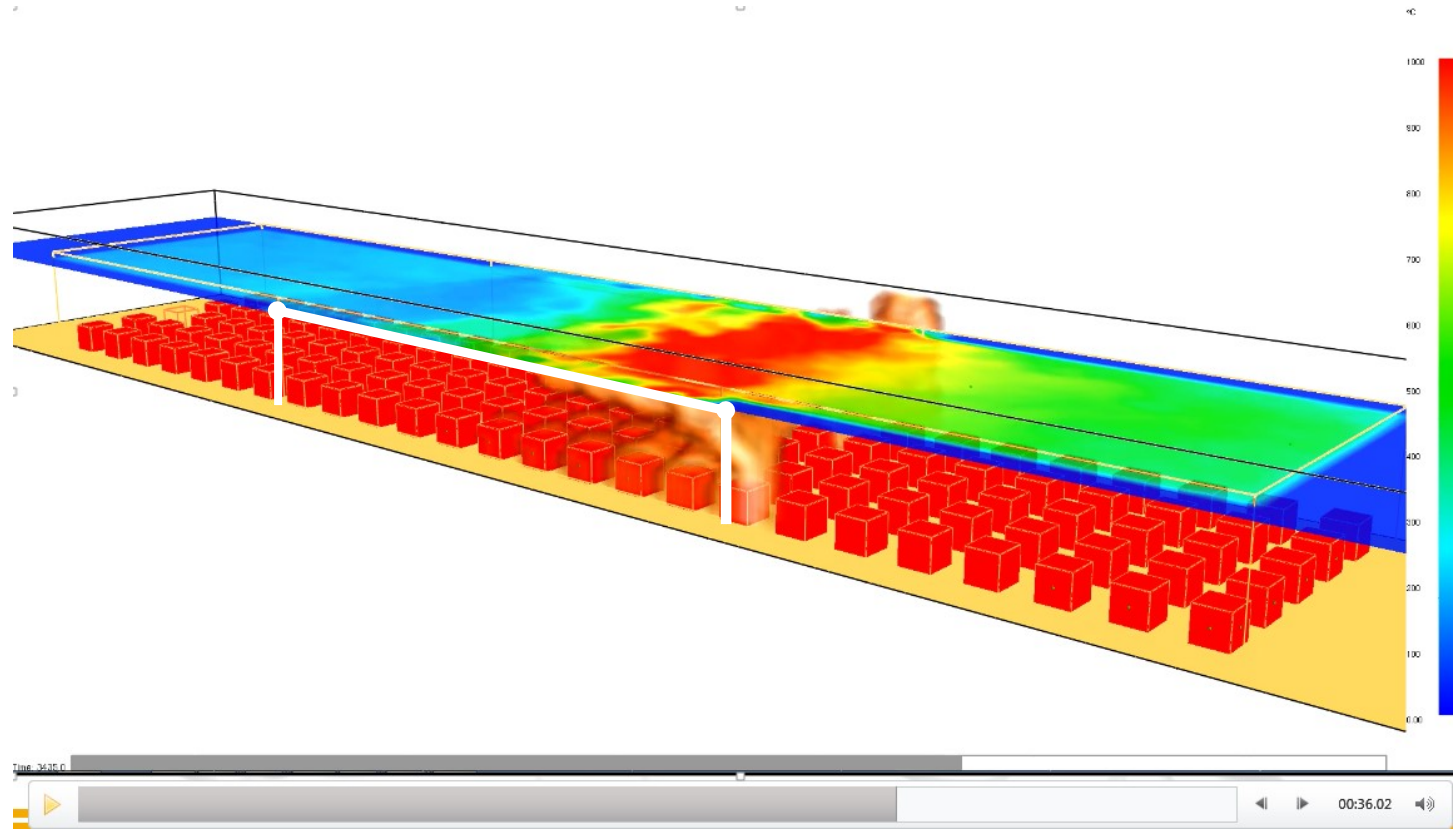
Xu Dai, Chang Liu, Weitian Lu, **Stephen Welch**



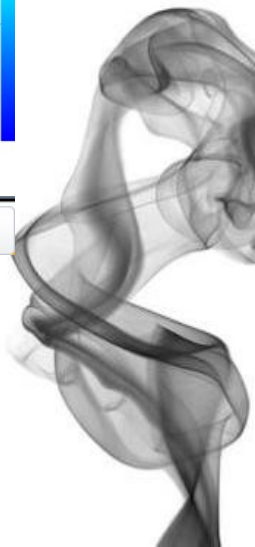
THE UNIVERSITY *of*  
EDINBURGH  
United Kingdom




# Travelling fires for structures



Charlier, M., Vassart, O., Gamba, A., Dai, X., Welch, S. & Franssen, J.-M. (2018) "CFD Analyses Used to Evaluate the Influence of Compartment Geometry on the Possibility of Development of a Travelling Fire", SiF 2018, University of Ulster, 6-8 June 2018

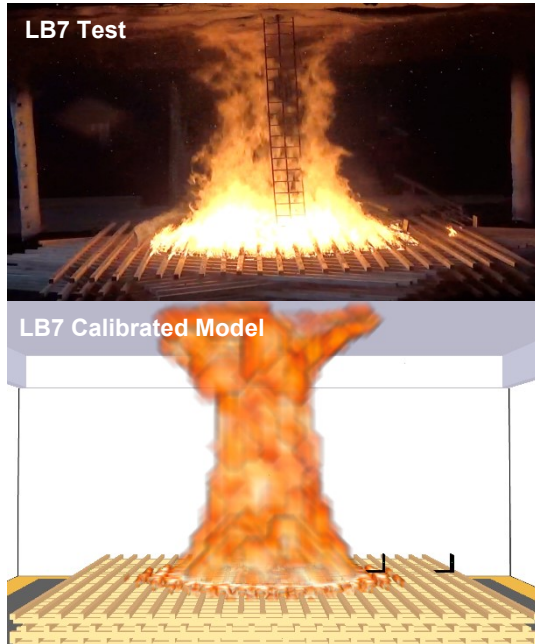




Jose Torero\*, Scaling-Up Fire:

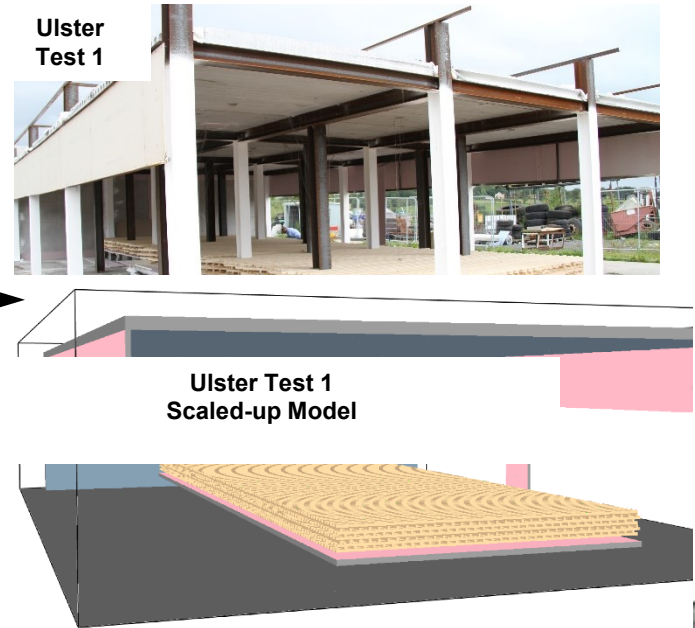
“The link between refinements in the combustion processes involved in fire modelling and the potential improvements in a fire safety strategy is generally blurred by the complexity of the processes involved, the natural incompatibility of time and length scales and the unavoidable scenario uncertainty. **In this context the use of CFD as a basis for the Scaling-Up of fire has a very clear gain.**”

# Research method



“Scaling-up”

All CFD model parameters remain the same except for compartment info





# Crib fire experiments

Gamba, Charlier & Franssen (2020) Propagation tests with uniformly distributed cellulosic fire load FSJ 103213 .pdf - Adobe Acrobat Reader DC

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Bookmarks

- Propagation tests with uniformly distributed cellulosic fire load
  - 1 Introduction
  - 2 First series of tests (LA)
    - 2.1 Ignition system
    - 2.2 Test description
    - 2.3 Measured quantities in the LA series
  - 3 Second series of tests (LB)
    - 3.1 Test description
    - 3.2 Measured quantities in the LB series
  - 4 Discussion
  - 5 Conclusions
  - CRedit authorship contribution statement
  - Declaration of competing interest
  - Acknowledgements
  - Appendix A Supplementary data
  - References

Fire Safety Journal 117 (2020) 103213

Contents lists available at ScienceDirect

Fire Safety Journal

journal homepage: <http://www.elsevier.com/locate/firesaf>

ELSEVIER

Propagation tests with uniformly distributed cellulosic fire load

Antonio Gamba<sup>a,\*</sup>, Marion Charlier<sup>b</sup>, Jean-Marc Franssen<sup>a</sup>

<sup>a</sup> Liege University, UEE Department, Belgium  
<sup>b</sup> ArcelorMittal Global R&D, Luxembourg

ARTICLE INFO

Keywords:  
 Natural fire tests  
 Fire spread  
 Fuel arrangement

ABSTRACT

In the recent past, the necessity to have a better understanding of fire dynamics and of the full structural response under real fires was the motivation for several large-scale non-standard fire tests. Nowadays, the novel need to better comprehend the fire dynamics behind the so called “travelling fires” underlined the limitations of those non-standard fire tests. The lack of standardised procedures does not allow making effective comparisons and drawing scientific conclusion from these tests. The fire group of Liege University performed eleven non-standard or “natural fire” tests within the context of the RFCS research project TRAFIR sponsored by the E.U. Commission (grant N°754,198). The aim of this experimental campaign was to determine a uniformly distributed fuel arrangement that would lead to a medium fire growth as recommended for office buildings in Eurocode 1. This paper presents the test results in terms of fire growth rate, flame length, temperature along the flame controlling

\* Gamba, A., Charlier, M. & Franssen, J.-M. (2020) “Propagation tests with uniformly distributed cellulosic fire load”, Fire Safety Journal 117, 103213 doi:10.1016/j.firesaf.2020.103213

## “Liege test series”, LB7 Test, Marchienne, Belgium, 2018

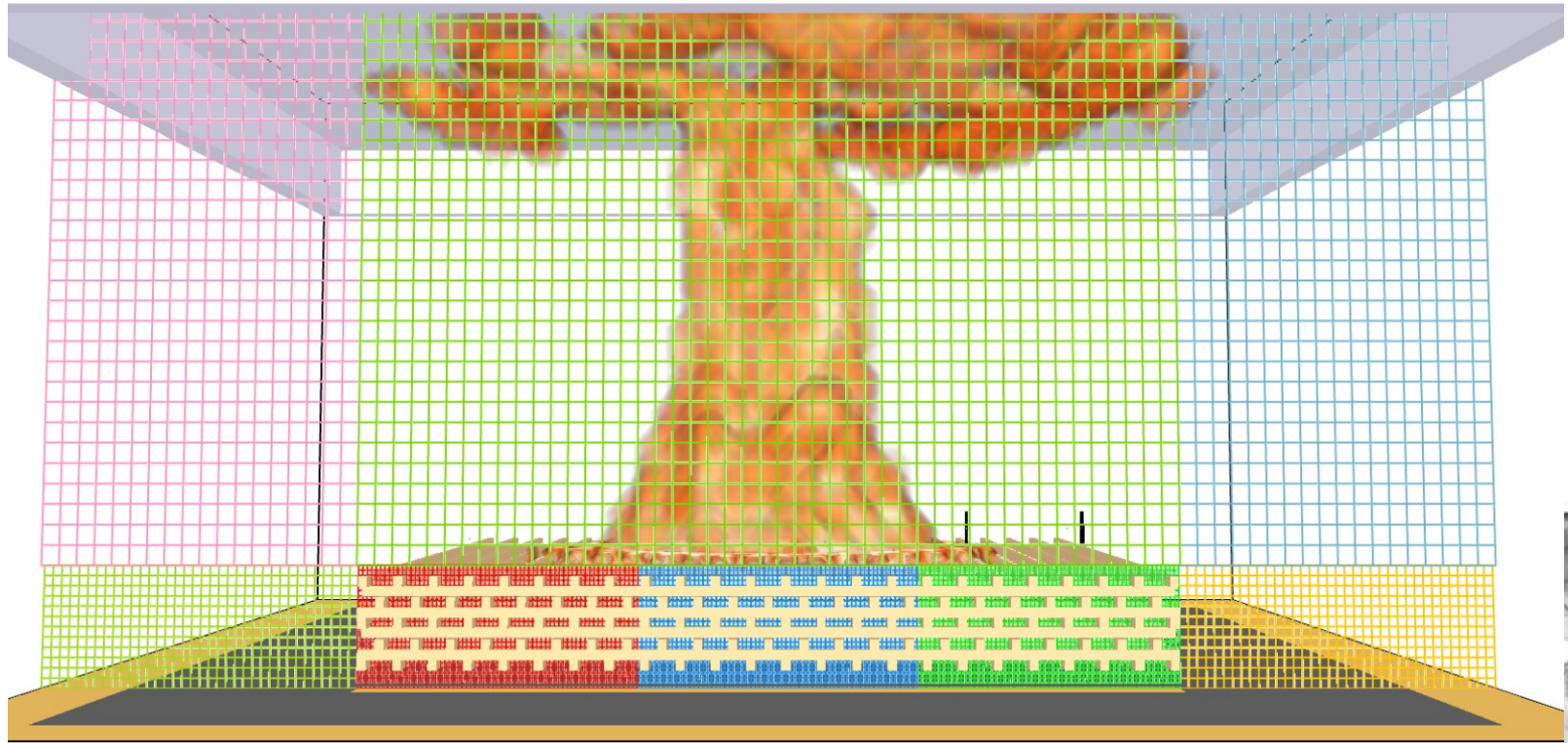
- Experimental arrangement



(a) Skewed view of test rig without wood sticks, and (b) Side view of test setup.

# FDS modelling for calibration, “Liege test series”, LB7\*

- Grid cell resolution in elevation view



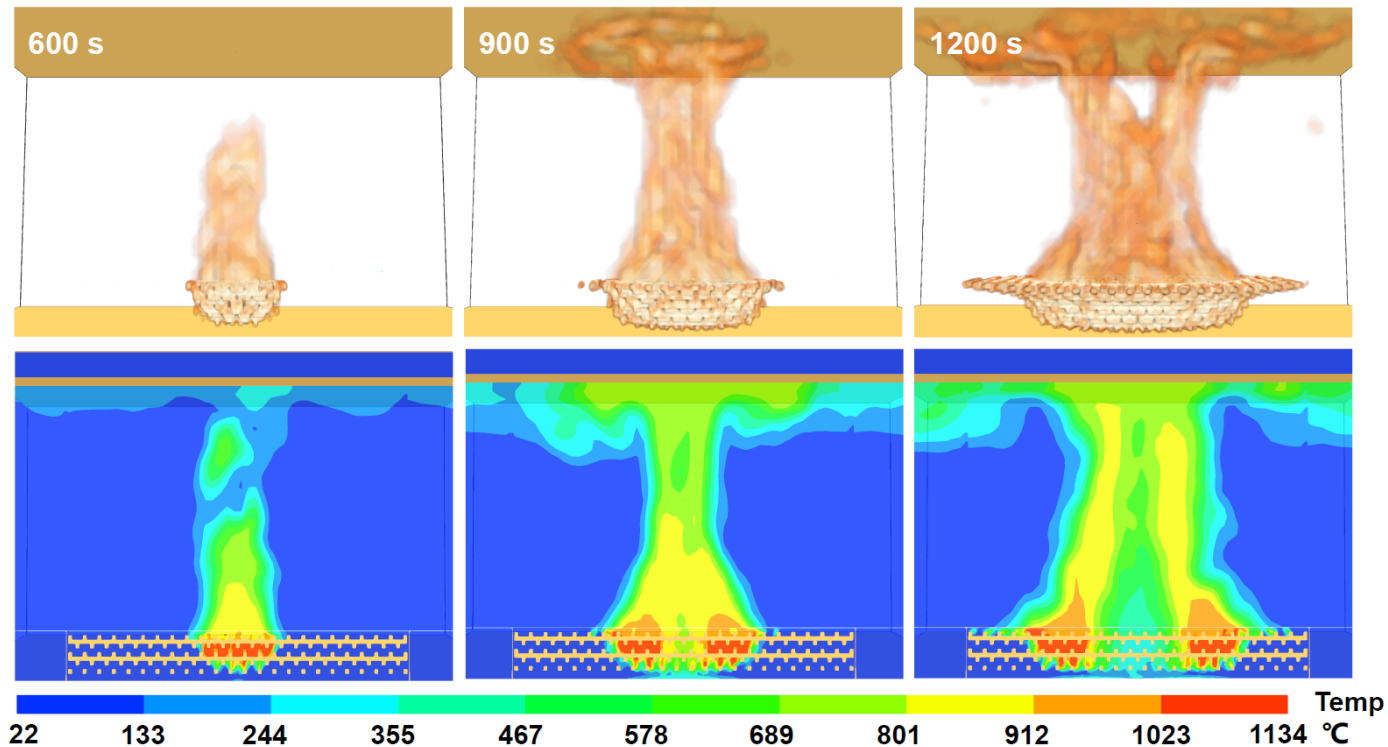
Grid cell resolution of the model:  $1.5 \times 1.5 \times 1.75$  cm per cell for wood sticks in porous crib structure,  $6 \times 6 \times 7$  cm and  $3 \times 3 \times 3.5$  cm cell size in gas phase, total no. cells ~1.3 million.

\* Dai, X., Gamba, A., Liu, C., Anderson, J., Charlier, M., Rush, D. & Welch, S. (2022) “An engineering CFD model for fire spread on wood cribs for travelling fires”, *Advances in Engineering Software* 173:103213 <https://doi.org/10.1016/j.advengsoft.2022.103213>



# FDS modelling for calibration, “Liege test series”, LB7

- Fire development within the wood crib
- Temperature development within the wood crib

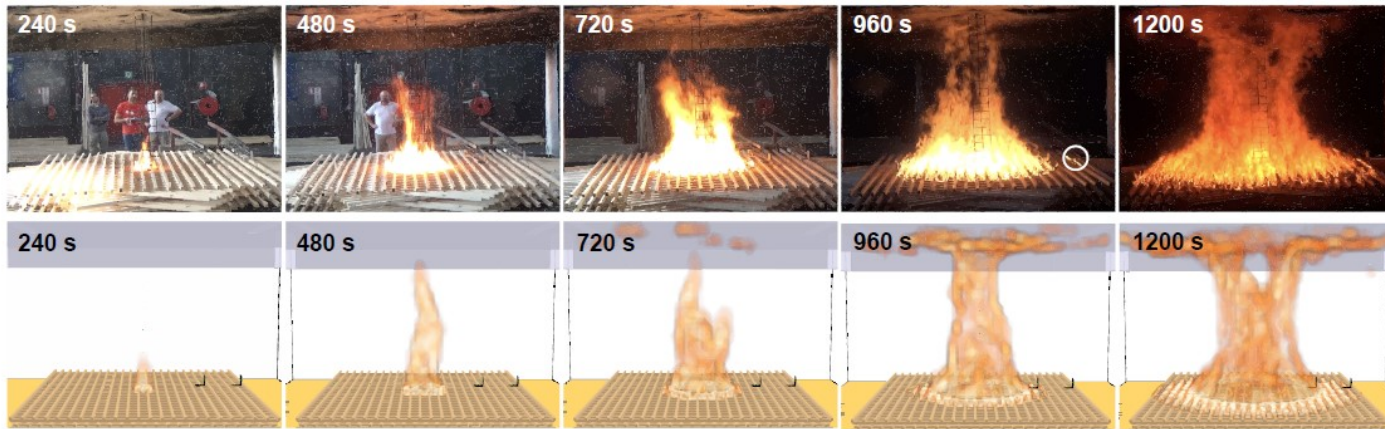


(a) Flame development within wood cribs (wood sticks “obstruction” removed in Smokeview for clearer flame demonstration), and (b) Temperature development at the compartment central ‘slice’.

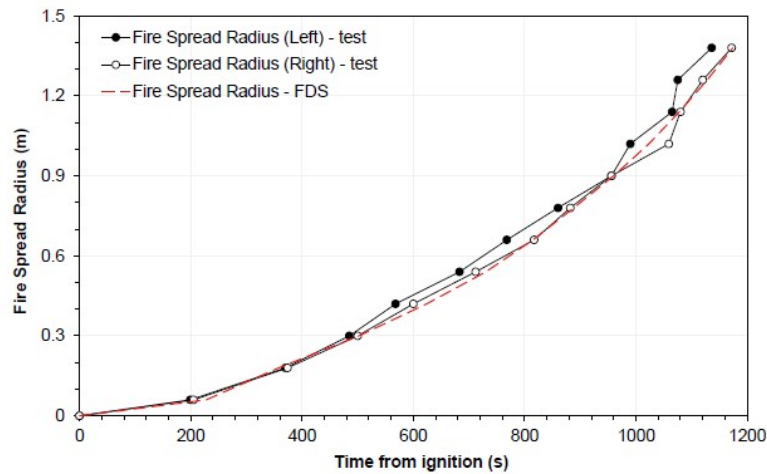




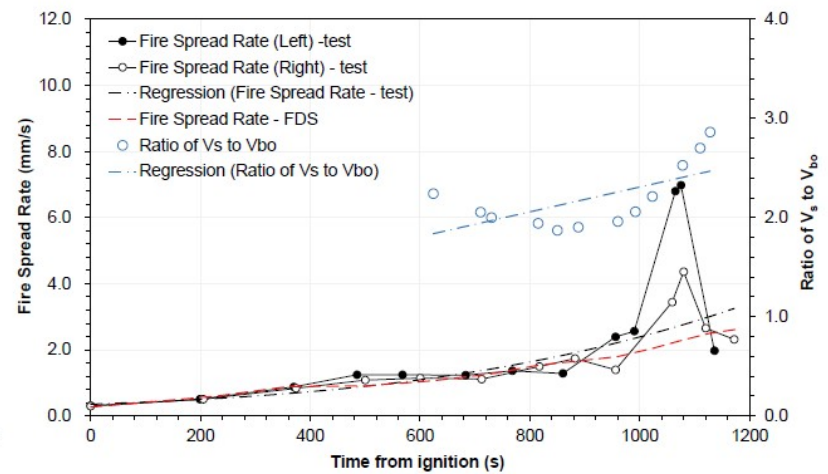
# FDS modelling for calibration, "Liege test series", LB7



Comparisons of the fire spread on top layer of wood cribs in FDS and LB7 test



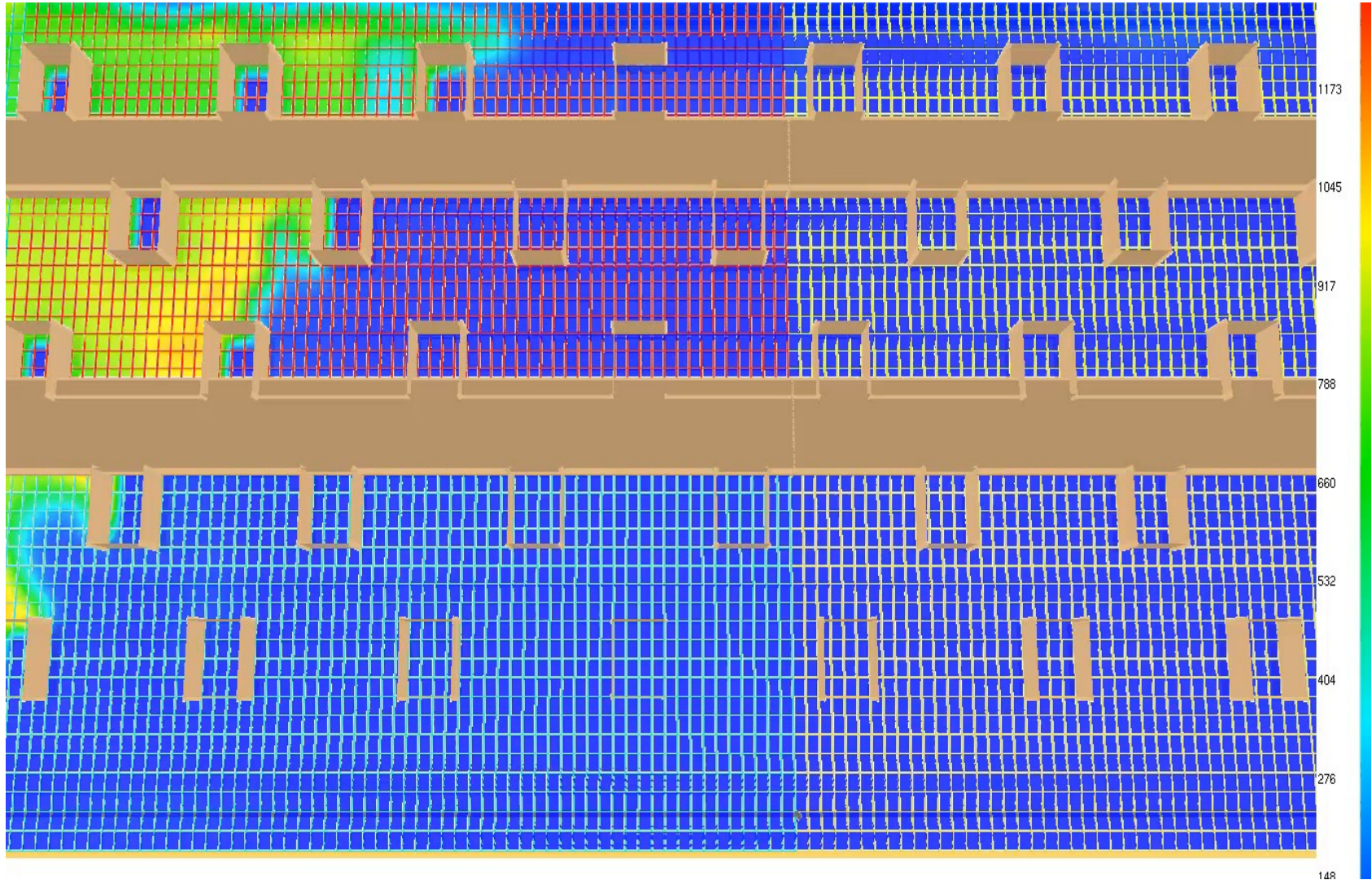
(a)



(b)

Comparisons between the FDS model and test: (a) evolution of the fire spread radius for the top layer of cribs; (b) calculated fire spread rate for the top layer of cribs

# FDS grid sensitivity studies, “Liege test series”, LB7





# Full scale experiments\*

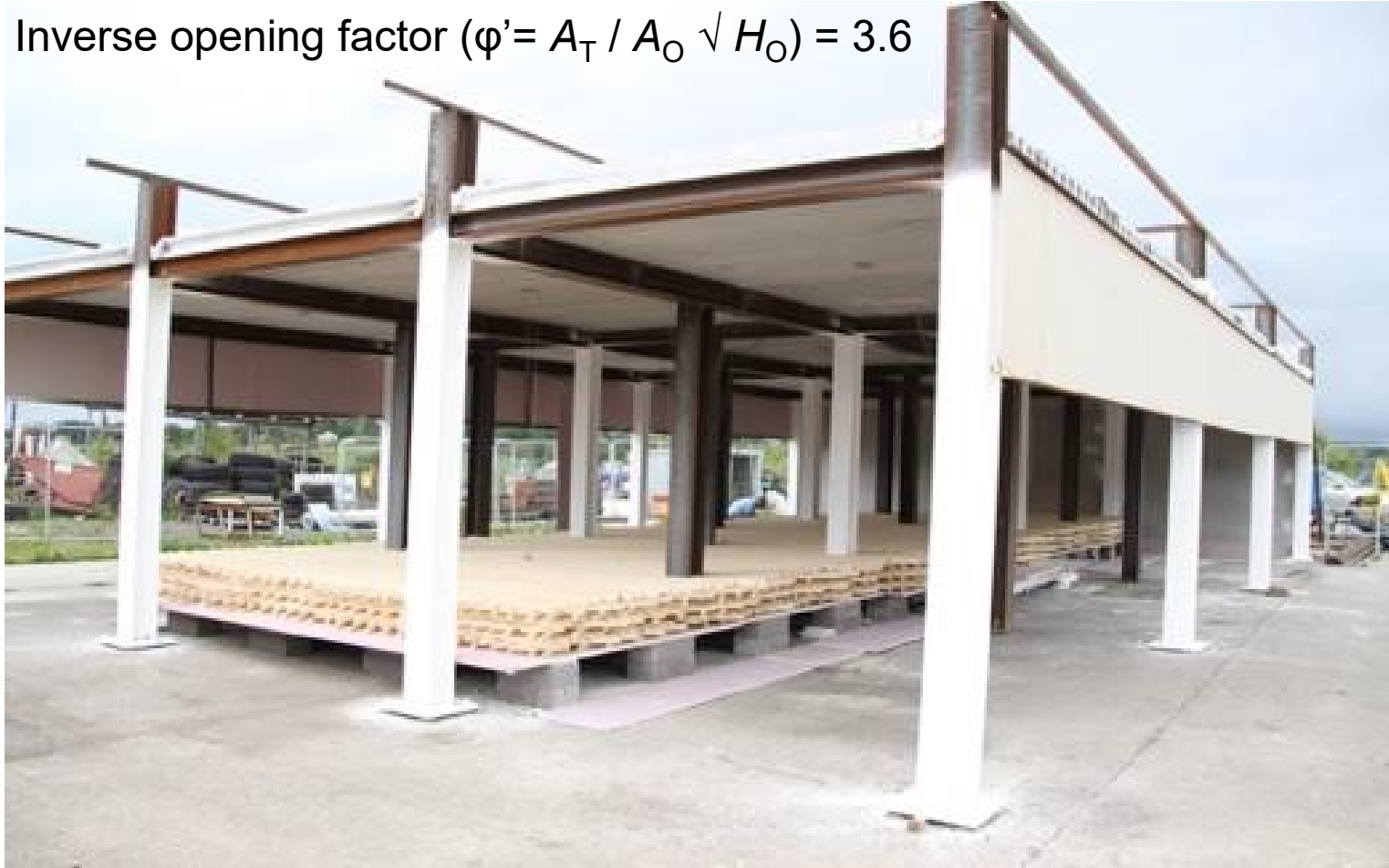


\* Nadjai, A., Naveed, A., Charlier, M., Vassart, O., Welch, S., Glorieux, A. & Sjöström, J. (2022) "Large scale fire test: The development of a travelling fire in open ventilation conditions and its influence on the surrounding steel structure", Fire Safety J., 130:103575 doi:[10.1016/j.firesaf.2022.103575](https://doi.org/10.1016/j.firesaf.2022.103575)

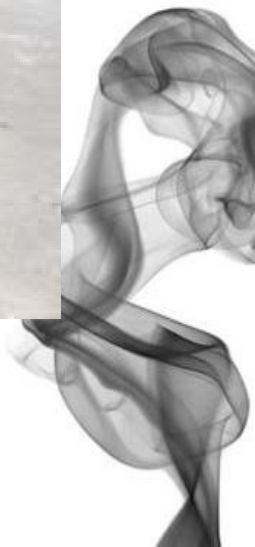


# TRAFIR Ulster test 1

Inverse opening factor ( $\phi' = A_T / A_O \sqrt{H_O}$ ) = 3.6



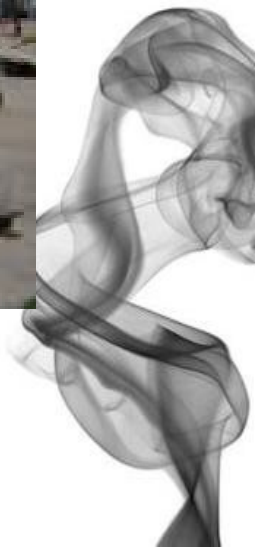
Nadjai, A., Naveed, A., Charlier, M., Vassart, O., Welch, S., Glorieux, A. & Sjöström, J. (2022)  
“Large scale fire test: The development of a travelling fire in open ventilation conditions and its influence on the surrounding steel structure”, Fire Safety J., 130:103575  
doi:[10.1016/j.firesaf.2022.103575](https://doi.org/10.1016/j.firesaf.2022.103575)





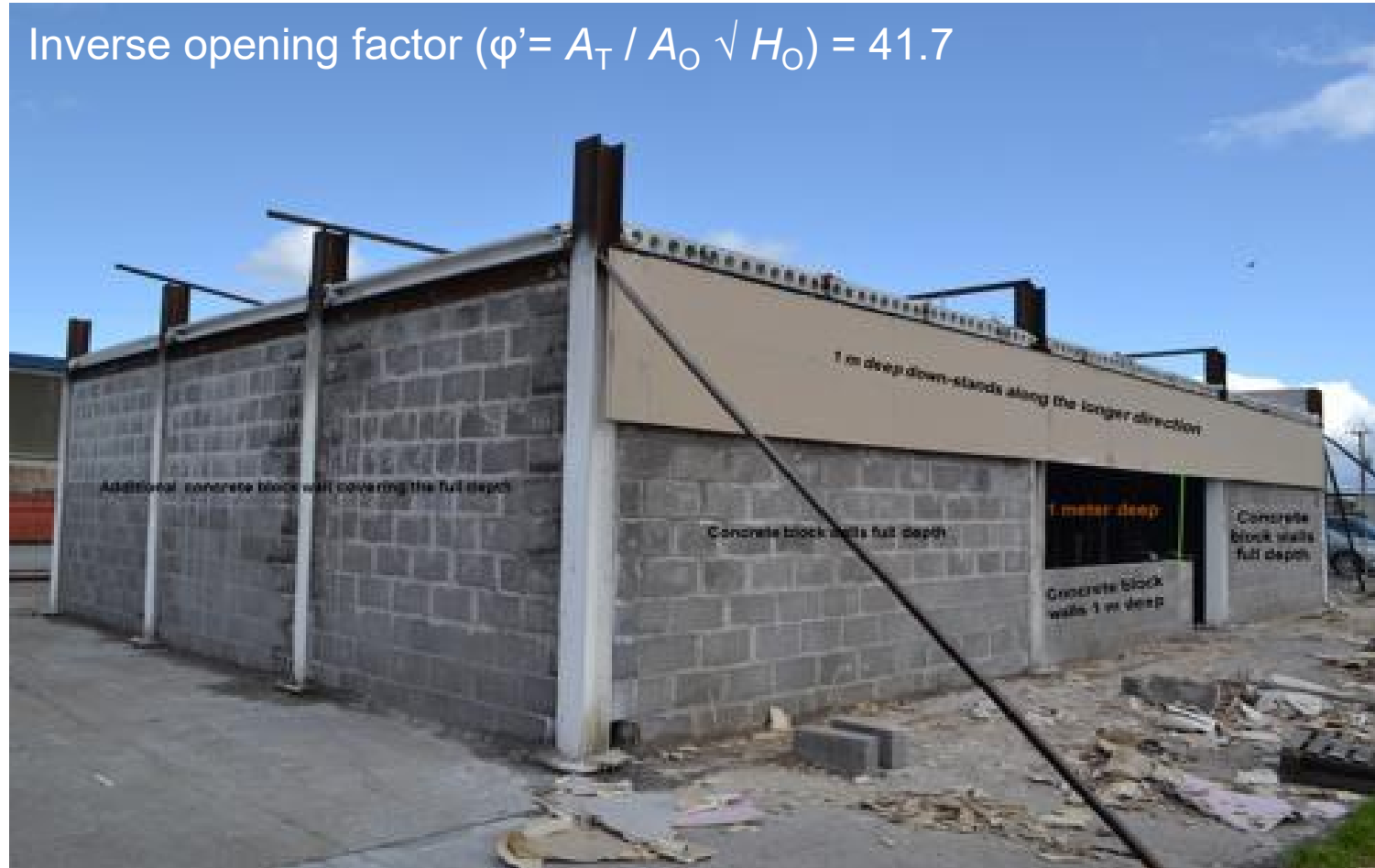
# TRAFIR Ulster test 2

Inverse opening factor ( $\phi' = A_T / A_O \sqrt{H_O}$ ) = 13.7



# TRAFIR Ulster test 3\*

Inverse opening factor ( $\phi' = A_T / A_O \sqrt{H_O}$ ) = 41.7

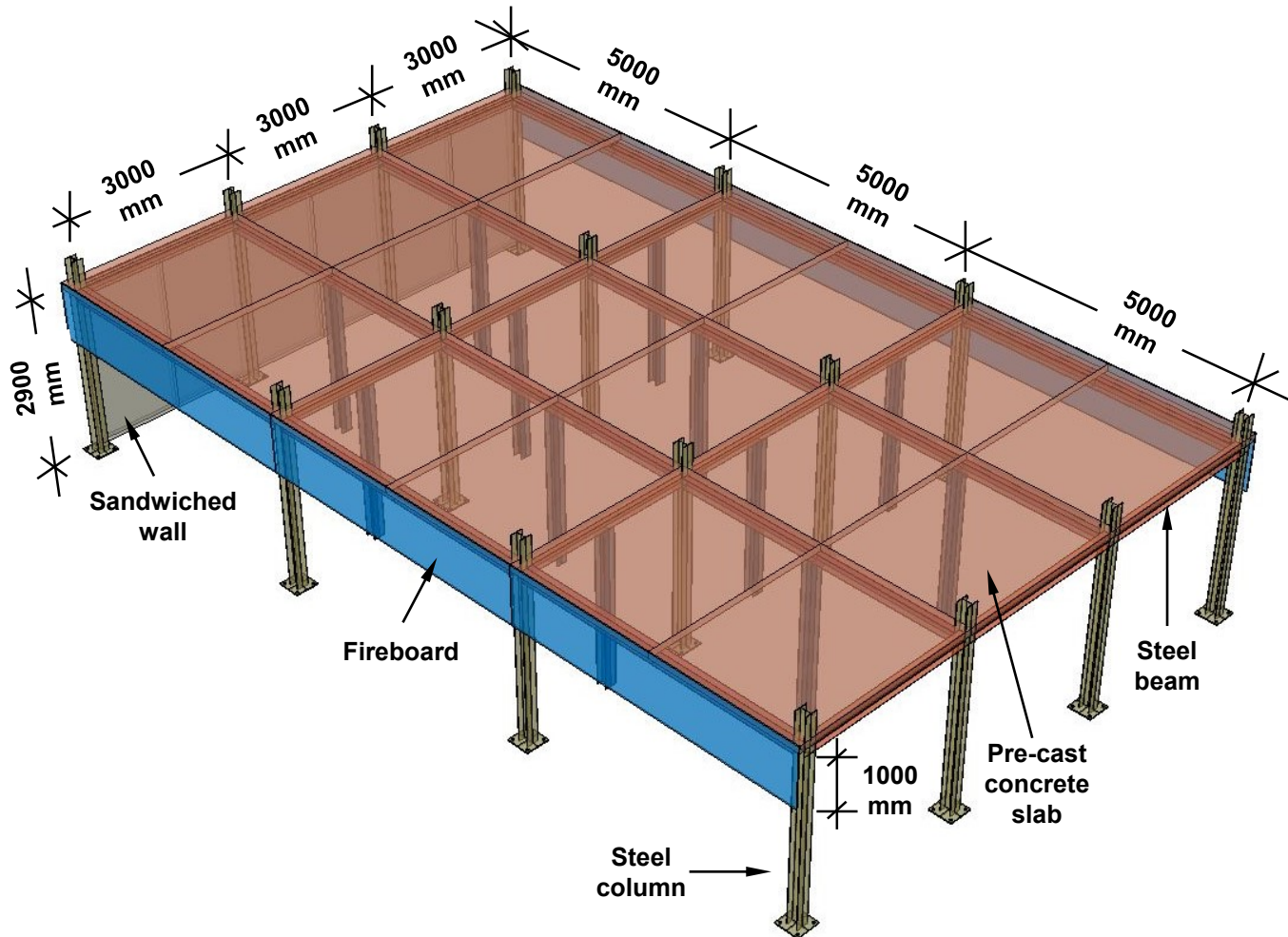


Alam, A., Nadjai, A., Charlier, M., Vassart, O., Welch, S., Sjöström, J. & Dai, X. (2022) "Large scale travelling fire tests with open ventilation conditions and their effect on the surrounding steel structure— The second fire test", J. Constr. Steel Res. 107032 doi:[10.1016/j.jcsr.2021.107032](https://doi.org/10.1016/j.jcsr.2021.107032)



# TRAFIR Ulster Travelling Fire Test 1

- Test compartment in 3D view:



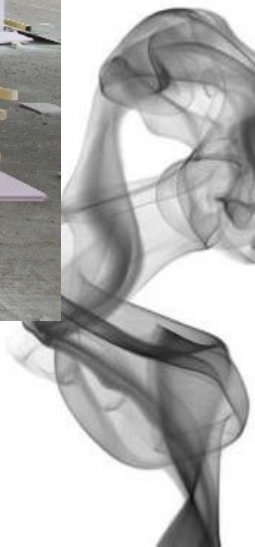
TRAFIR Ulster Travelling Fire Test 1, compartment in 3D view



# TRAFIR Ulster Travelling Fire Test 1



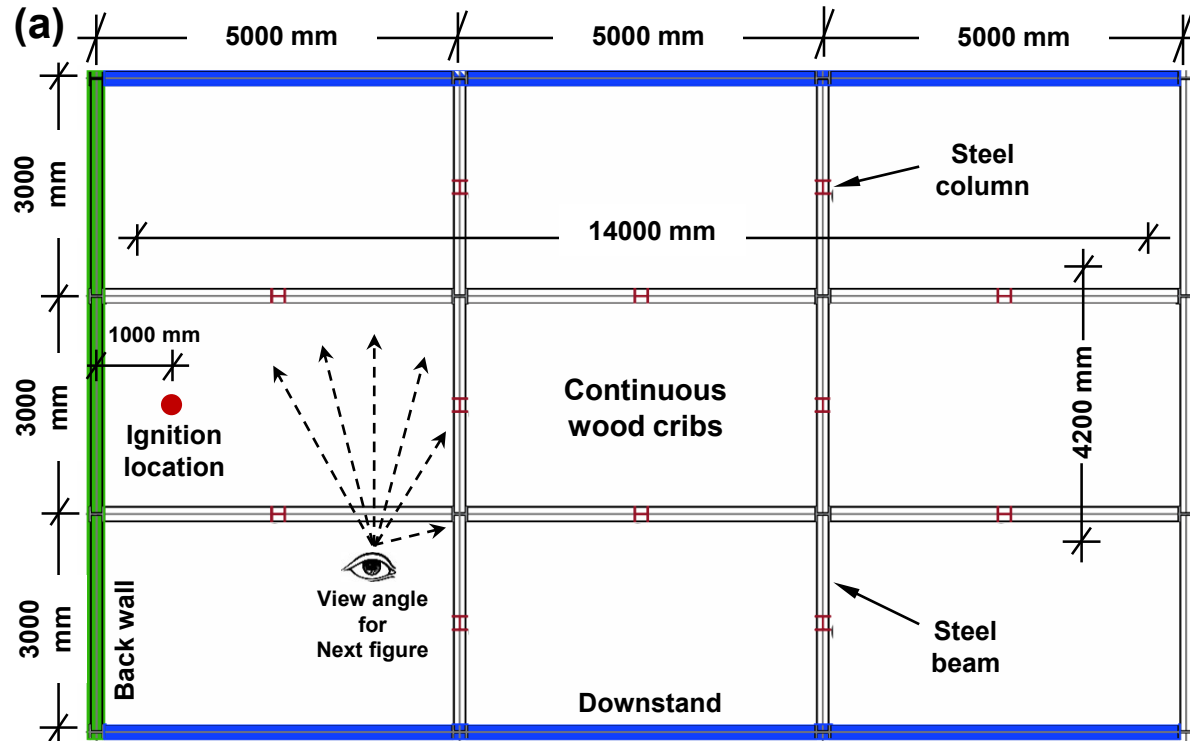
Nadjai, A., Naveed, A., Charlier, M., Vassart, O., Welch, S., Glorieux, A. & Sjöström, J. (2022)  
“Large scale fire test: The development of a travelling fire in open ventilation conditions and its influence on the surrounding steel structure”, Fire Safety J., 130:103575  
doi:[10.1016/j.firesaf.2022.103575](https://doi.org/10.1016/j.firesaf.2022.103575)





# TRAFIR Ulster Travelling Fire Test 1

- Wood sticks arrangement:

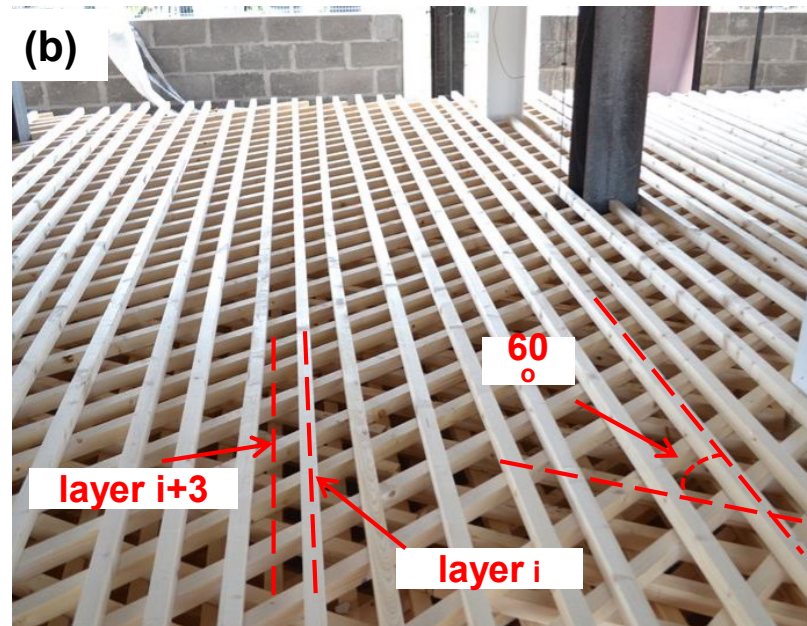


Wood sticks arrangement, (a) Layout in the compartment.

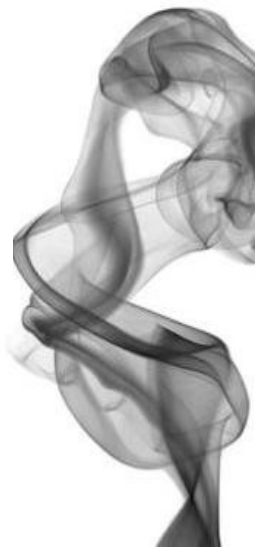


# TRAFIR Ulster Travelling Fire Test 1

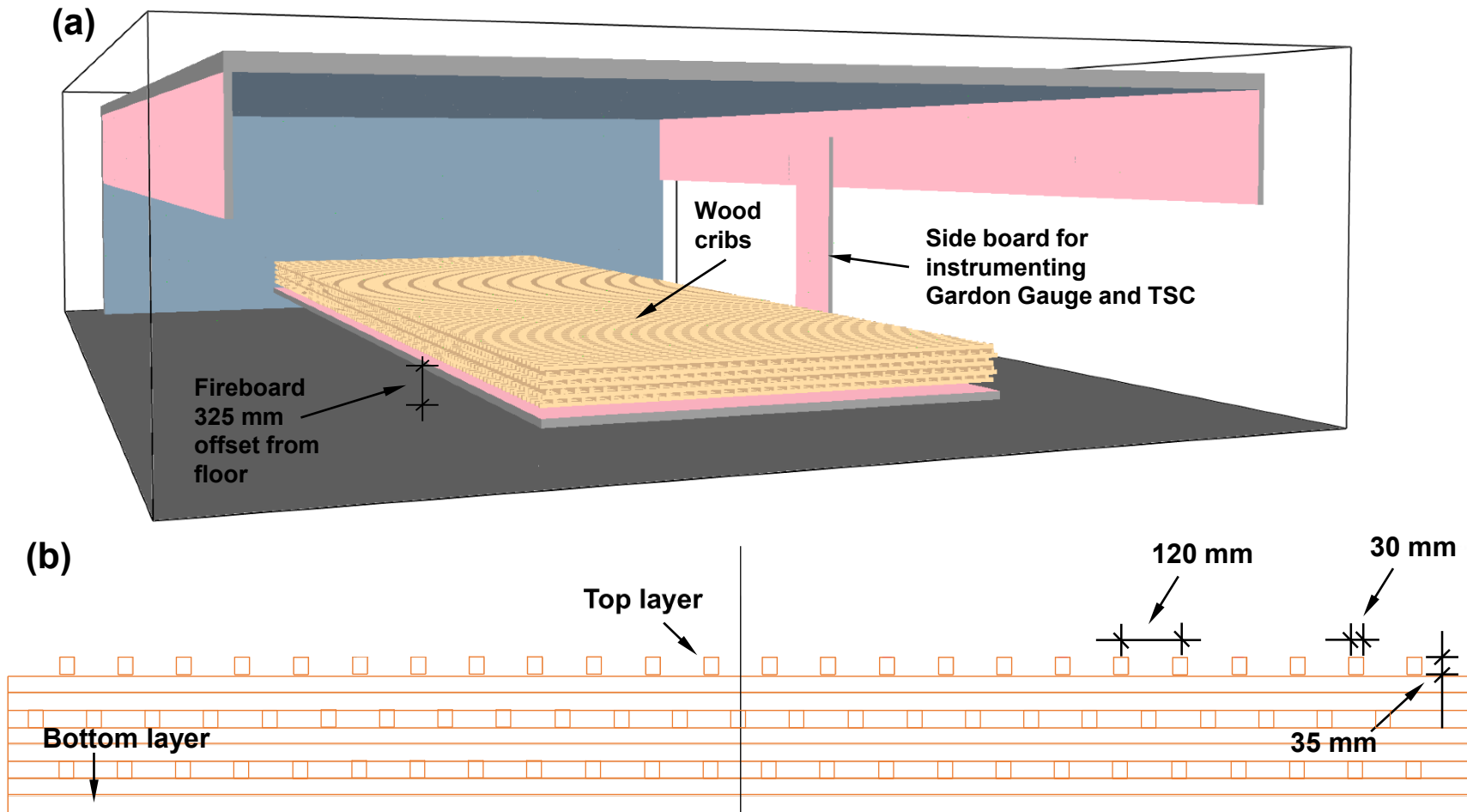
- Crib structure



Wood sticks arrangement, (b) Wood sticks orientation shifted 60° every layer, and for every three layers shifted horizontally for half of the wood stick pitch, same arrangement as the LB7 test from Gamba et al. [xx].



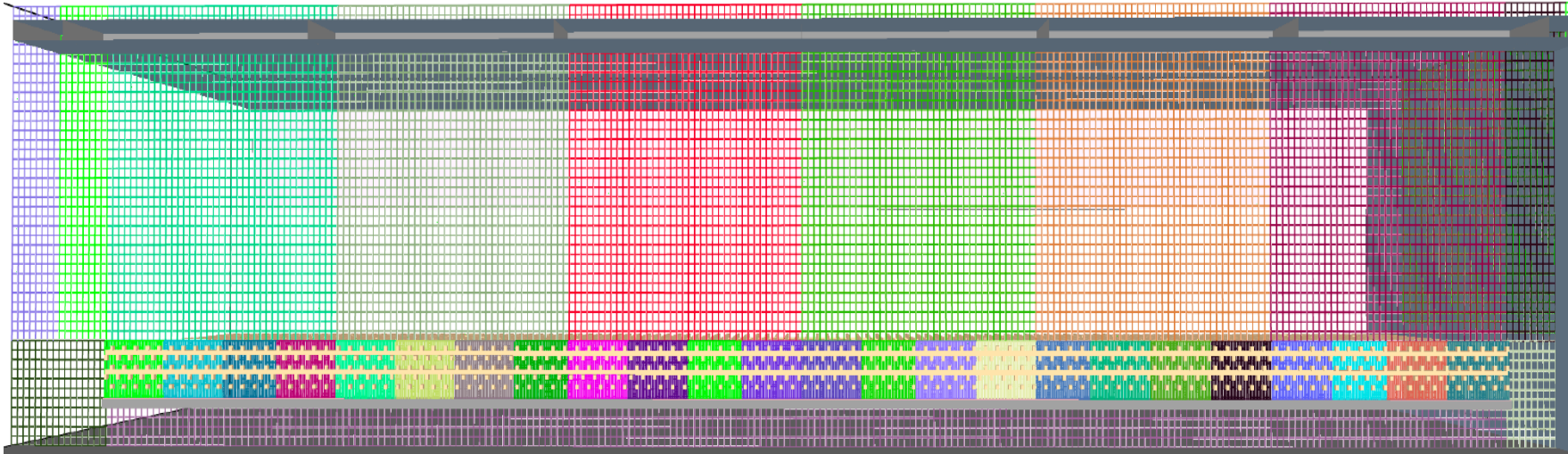
# “Scaled-up” CFD Model – TRAFIR Ulster test 1



“Scaled-up” CFD model, (a) Skewed view, and (b) Representation of the wood sticks in side-elevation view.

# “Scaled-up” CFD Model – TRAFIR Ulster test 1

- Grid cell resolution in elevation view



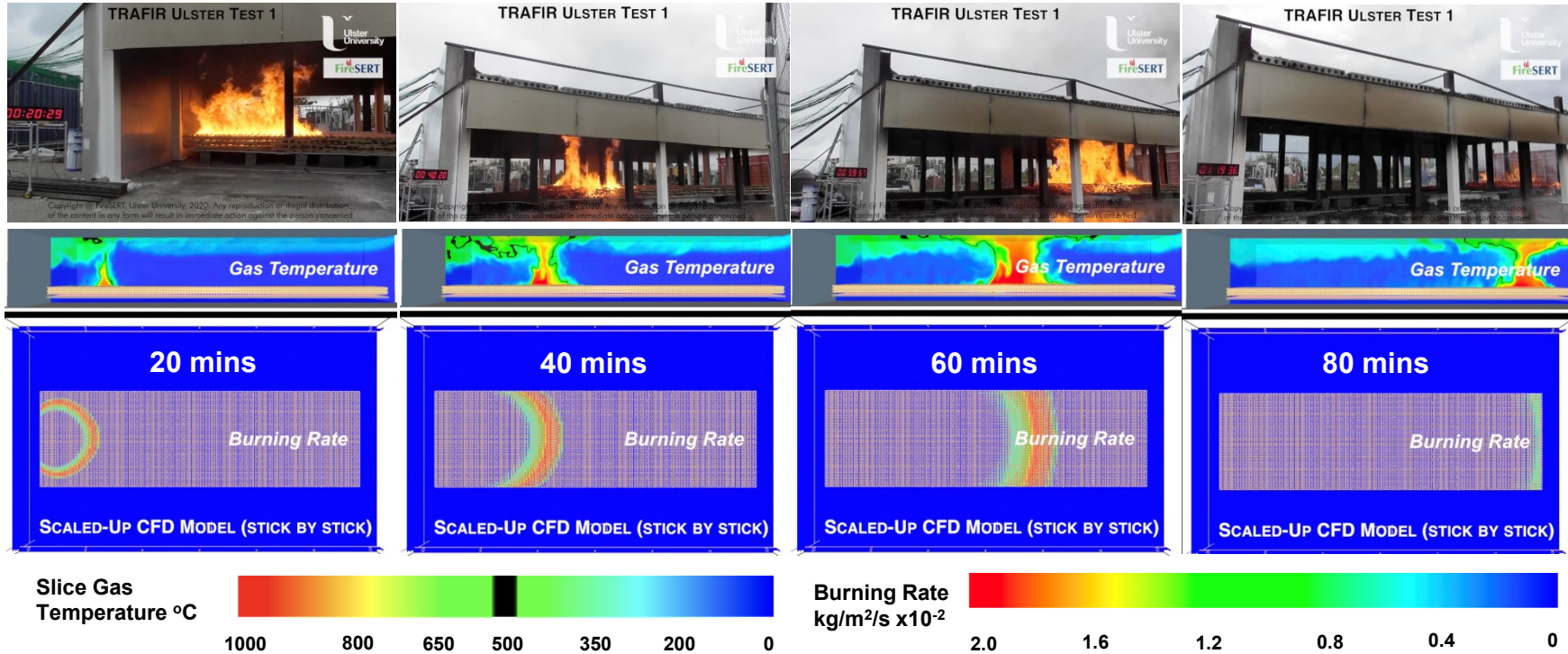
Grid cell resolution of the model:  $15 \times 15 \times 17.5$  mm per cell for the wood sticks at solid phase,  $60 \times 60 \times 70$  mm and  $30 \times 30 \times 35$  mm cell size at the gas phase, total no. cells ~8.3 million, with 125 meshes.





# Model Prediction vs. Test Results

## Fire development comparison



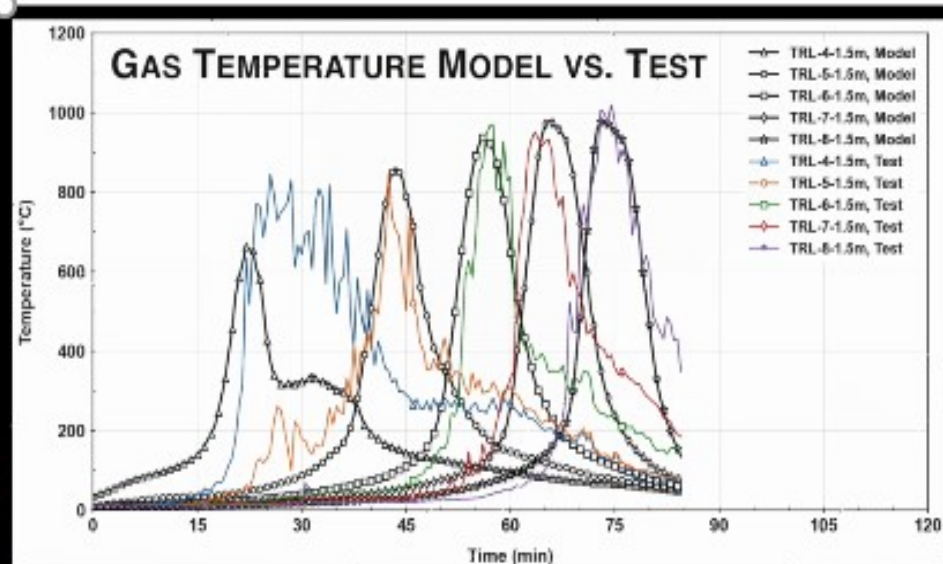
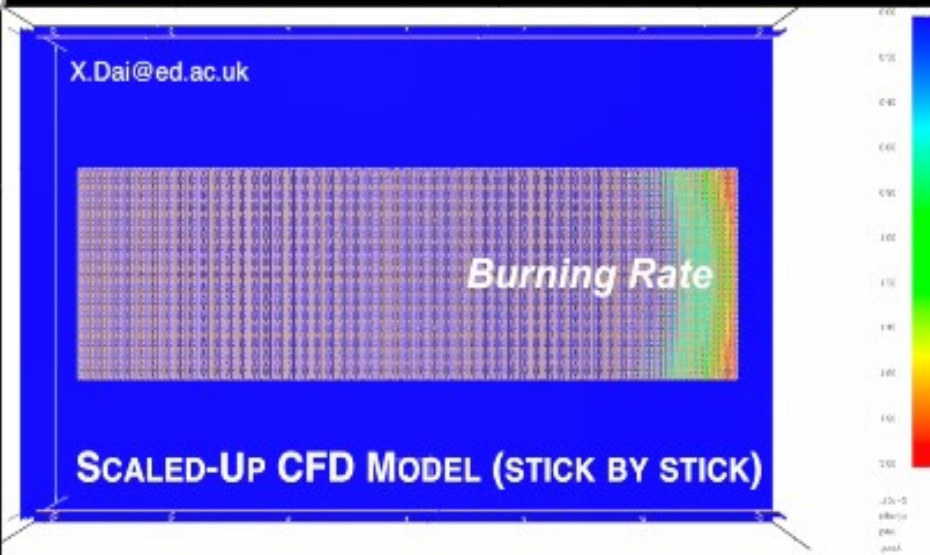
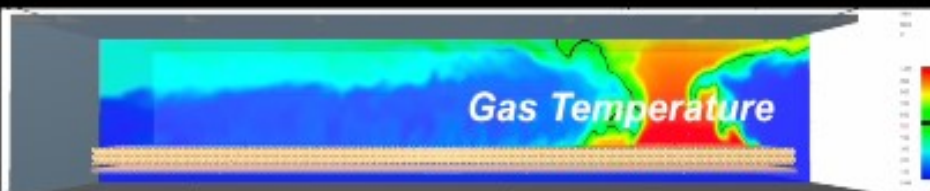
Scaled-up CFD model predicted fire spread comparison with the test, at 20, 40, 60 and 80 mins

# Model Prediction vs. Test Results

**77 min**

SCALING-UP:

FIRE SPREAD ON WOOD CRIBS (STICK BY STICK) USING CFD



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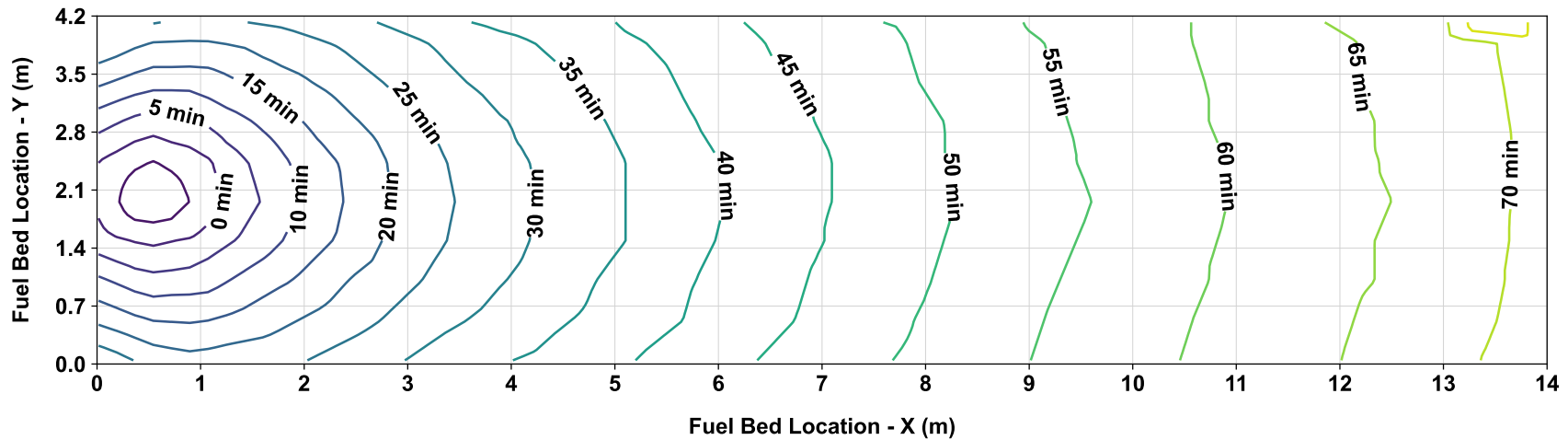


01:35.00



# Further Understanding on Test via Model in-depth Characterisation

## ○ Fire Spread Contour



Fire spread development with 5 mins intervals, interpreted from the model

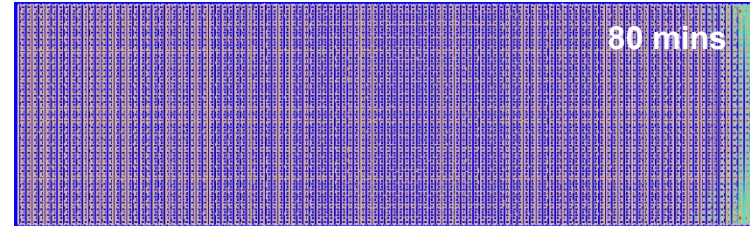
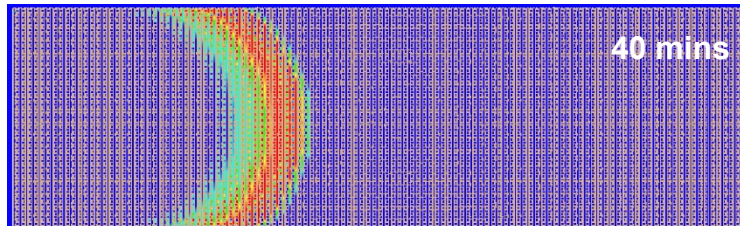
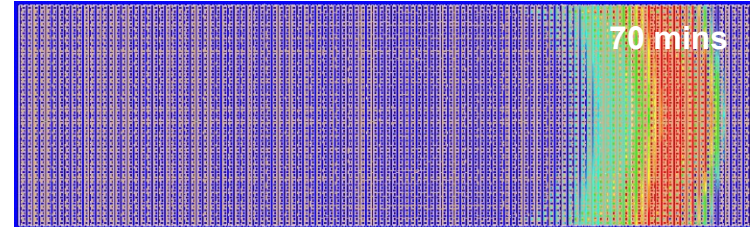
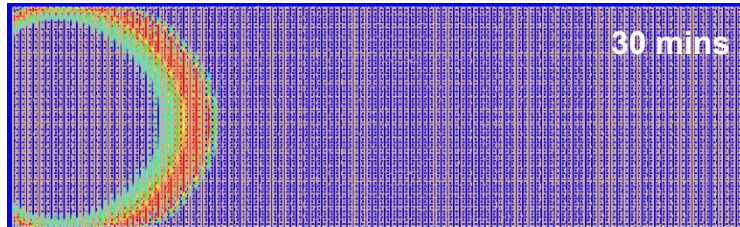
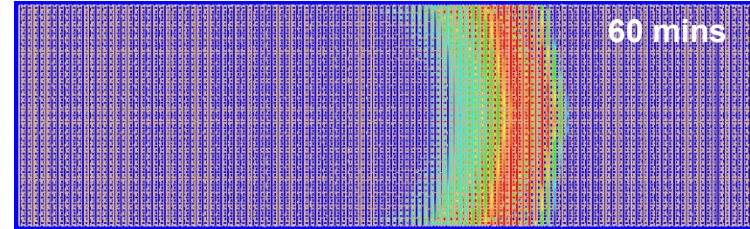
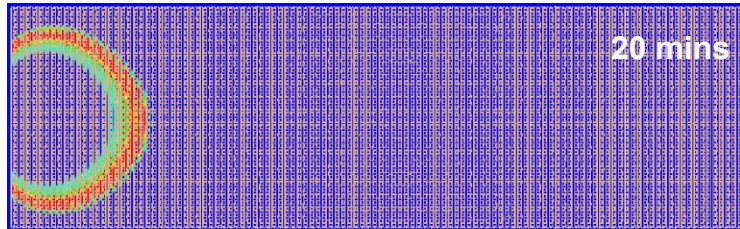
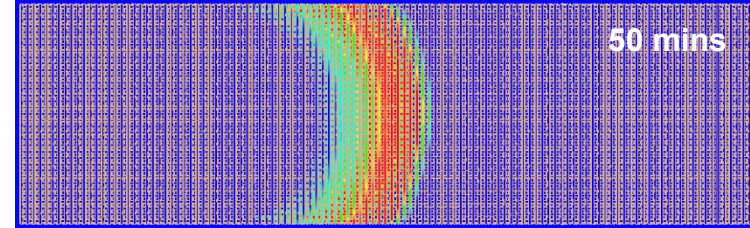
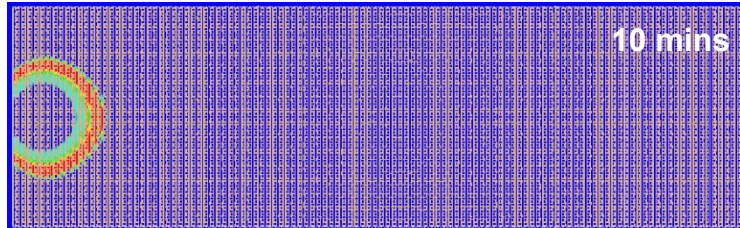
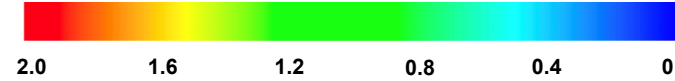




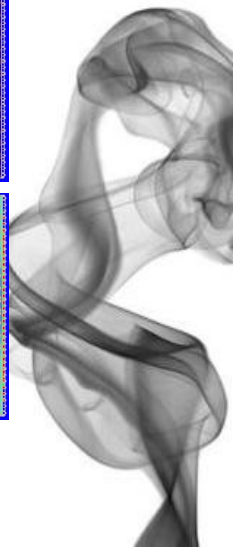
# Further Understanding on Test via Model in-depth Characterisation

## ○ Fire Spread Contour

Burning Rate  
 $\text{kg/m}^2/\text{s} \times 10^{-2}$

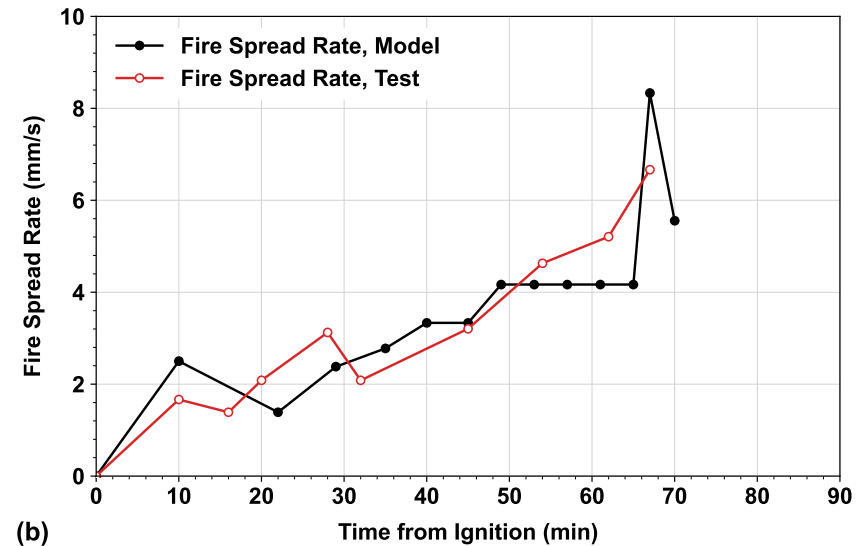
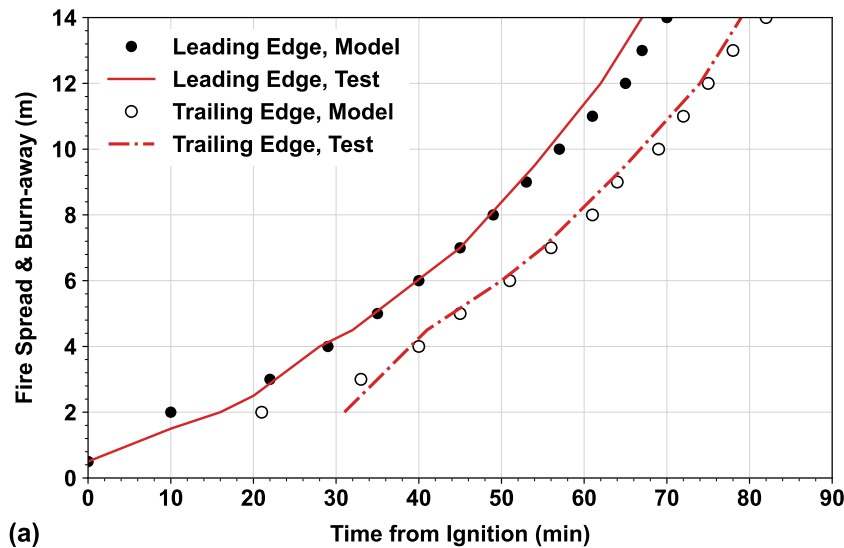


Burning rate of the continuous fuel bed with 10 mins intervals



# Model Prediction vs. Test Results

## ○ Fire spread & burn-away comparison



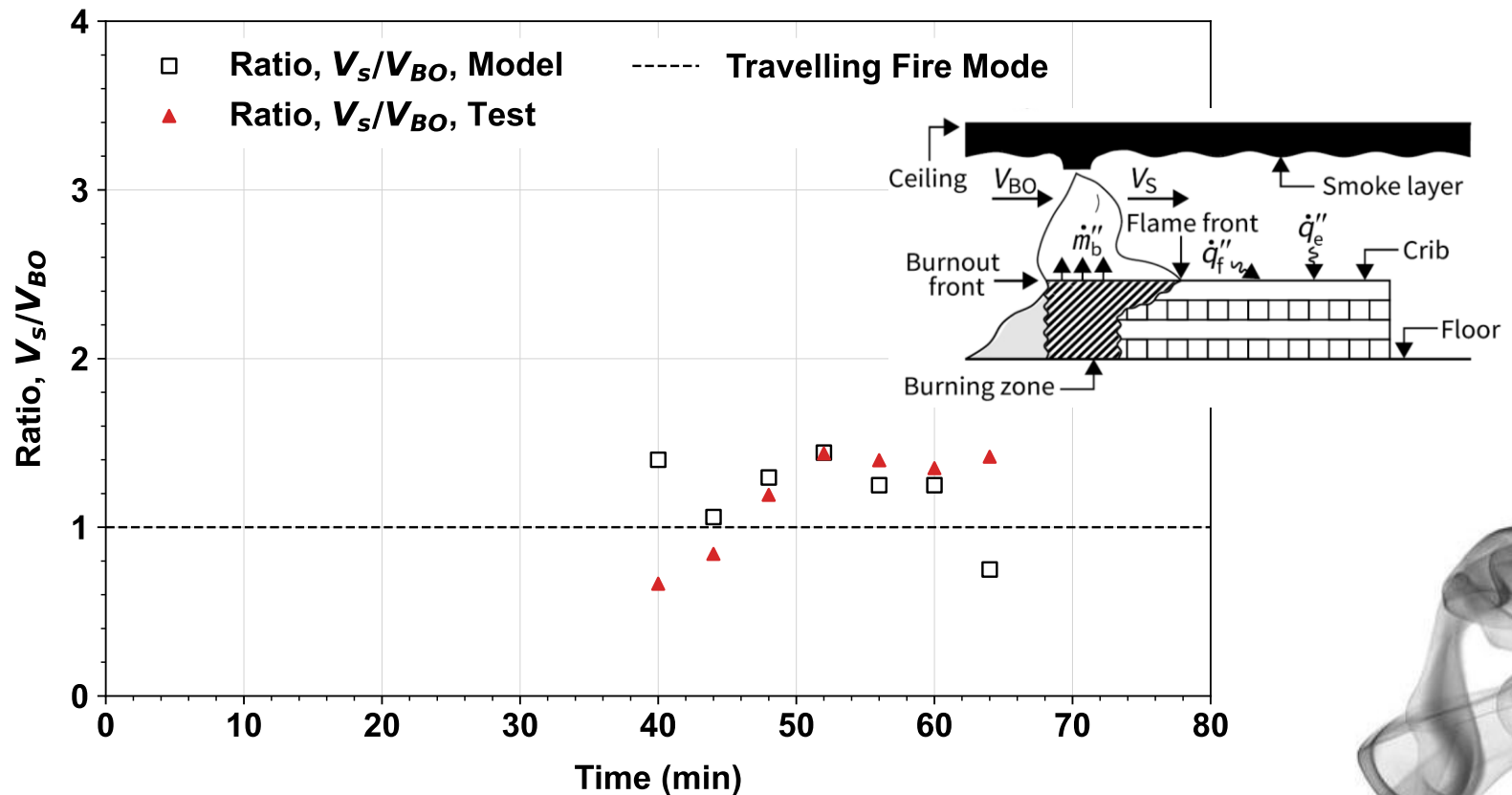
Comparison between the test and the model at compartment centreline along fire trajectory, (a) Fire spread distance & burn-away, and (b) Fire spread rate.





# Model Prediction vs. Test Results

## Fire mode comparison

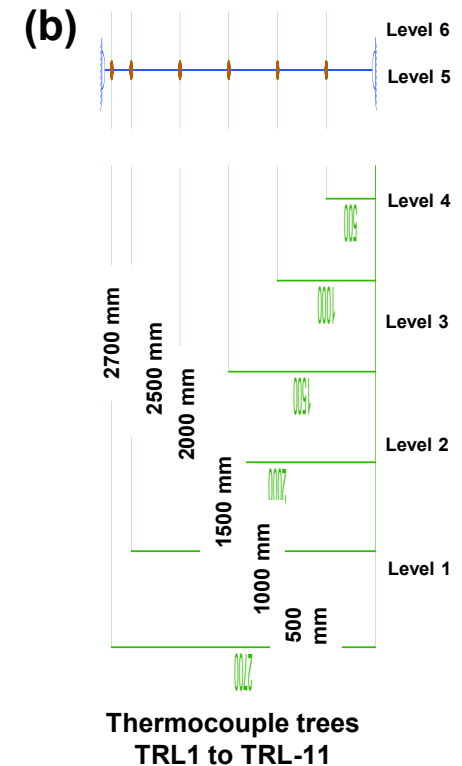
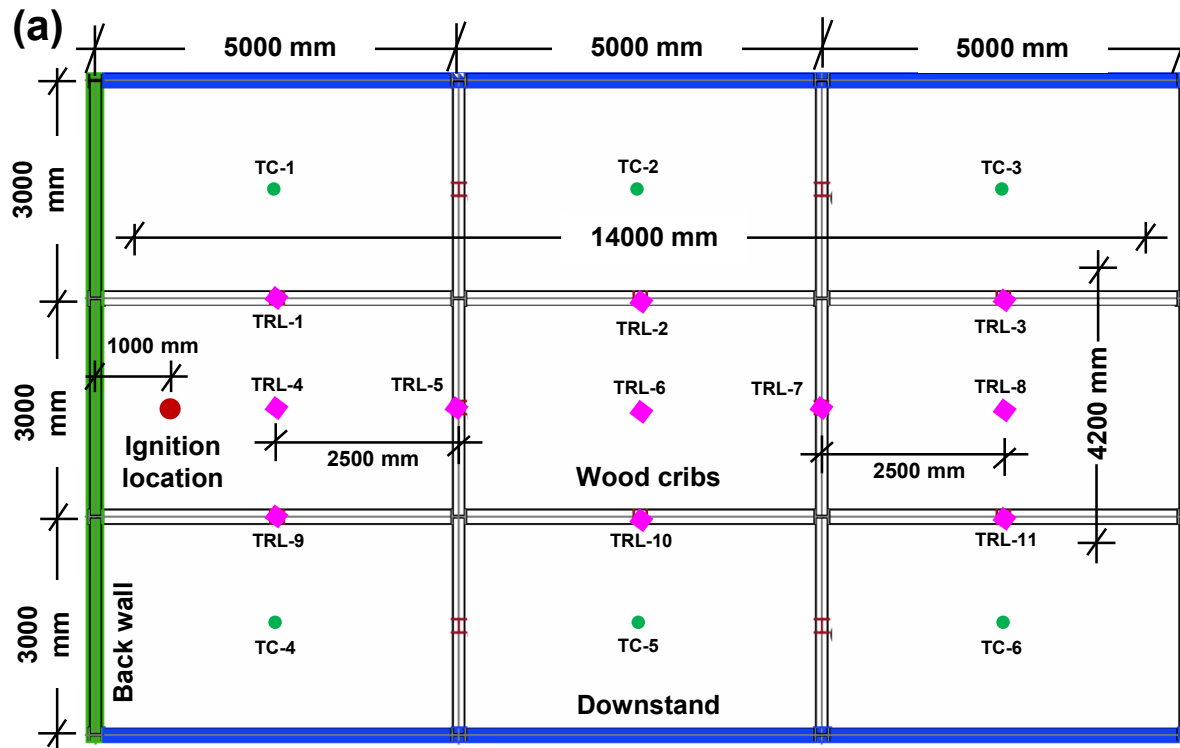


Comparison on fire mode parameter,  $V_s/V_{BO}$ : velocity of the flame spread front to velocity of the flame burnout front.



# Model Prediction vs. Test Results

## Thermocouple Temperatures



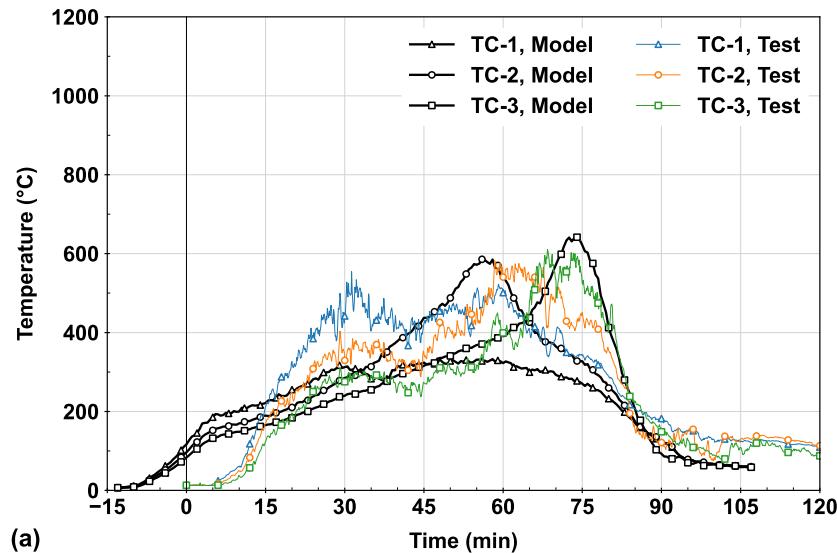
Location of the thermocouples for measuring gas phase temperatures, (a) plan view, TC-1 to TC-6 were thermocouples 200 mm below ceiling, (b) elevation view, TRL-1 to TRL-11 were thermocouple trees above the wood cribs.



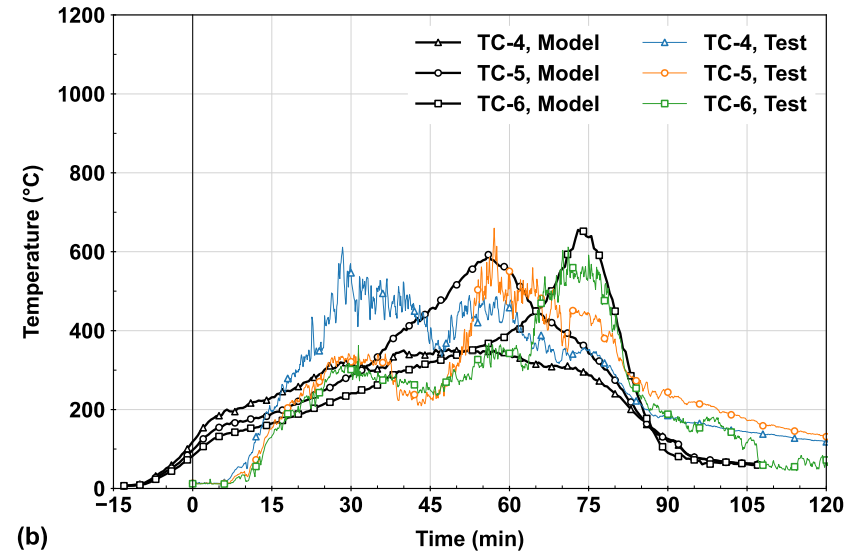
# Model Prediction vs. Test Results

## Gas Phase Temperatures – symmetry near ceiling

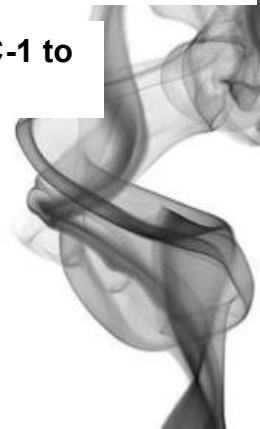
### Left external bays



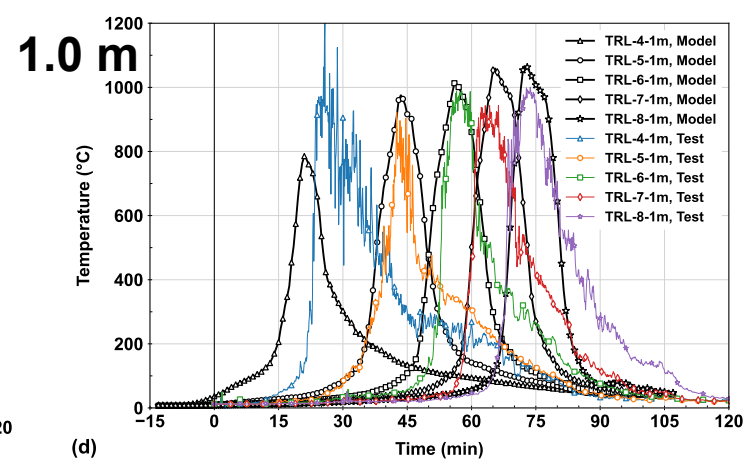
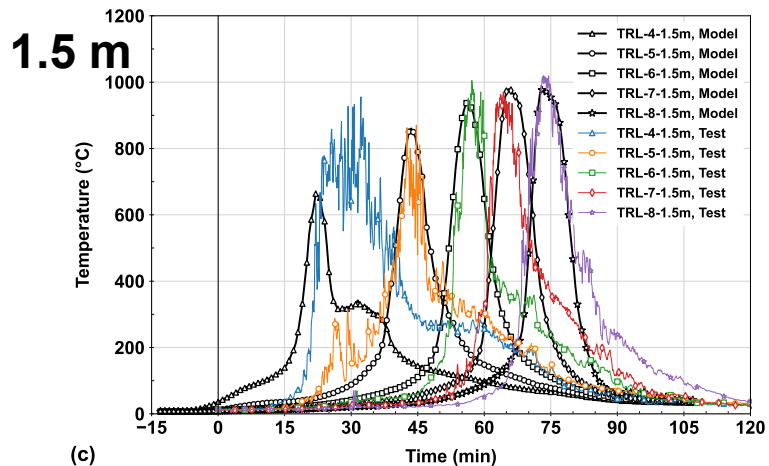
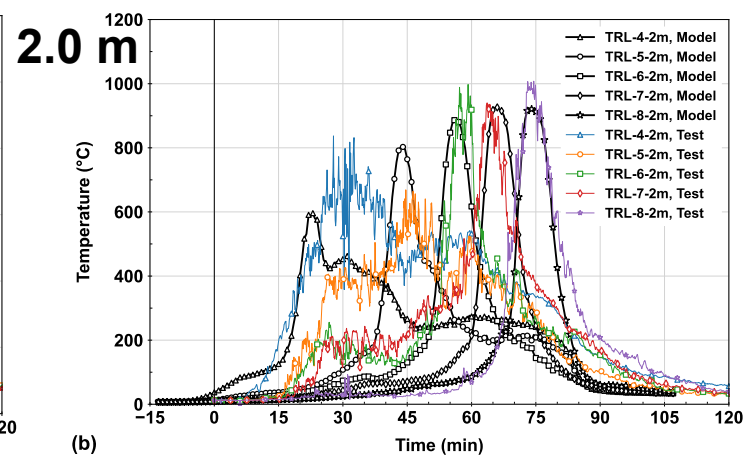
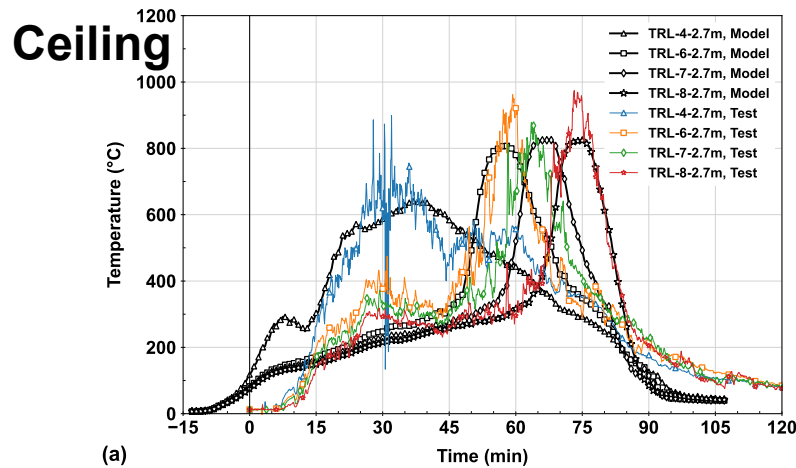
### Right external bays



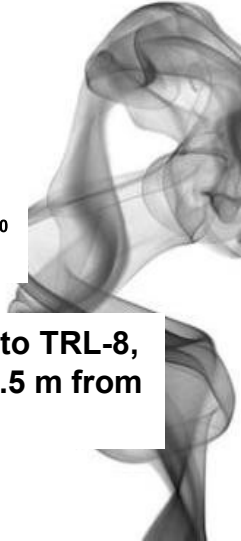
Comparison of the thermocouple temperatures, 200 mm from the ceiling level at side bays, (a) TC-1 to TC-3, and (b) TC-4 to TC-6.



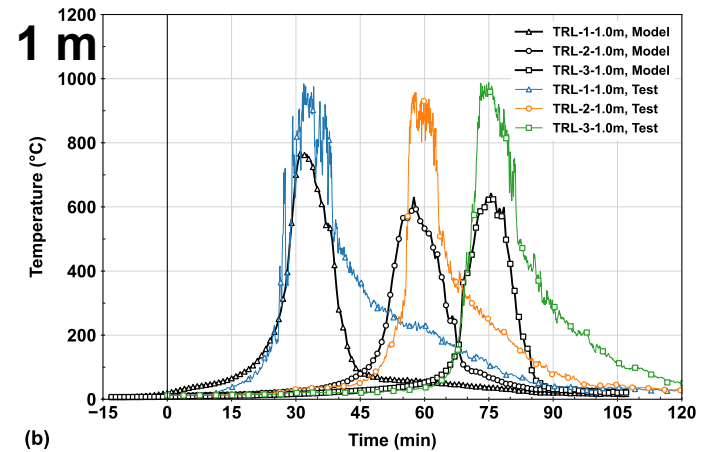
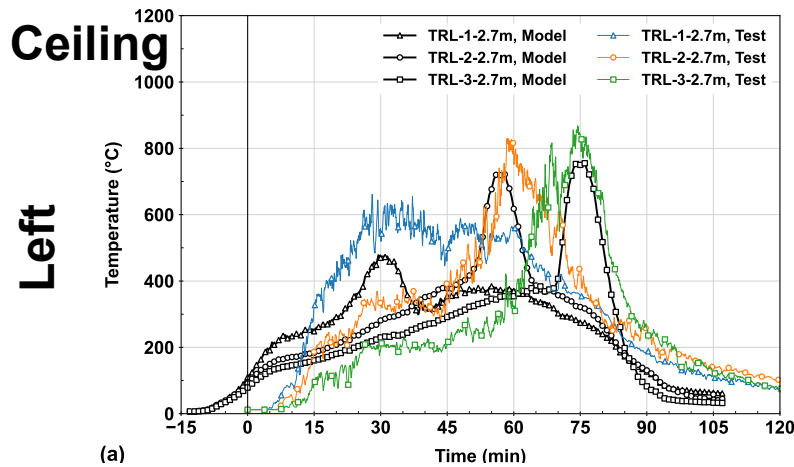
# Model Prediction vs. Test Results



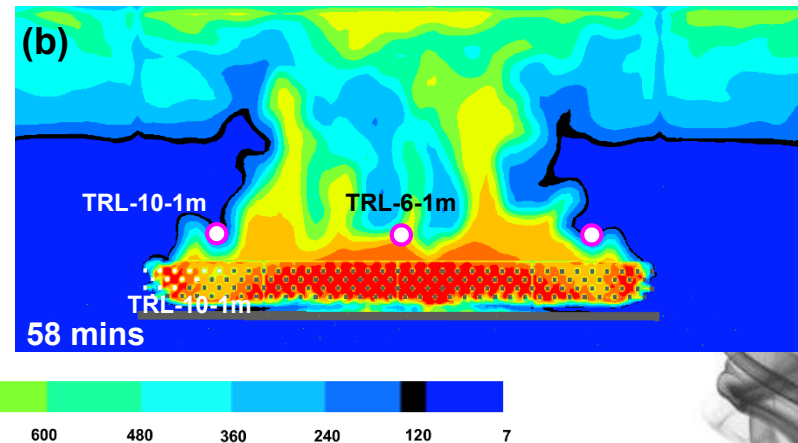
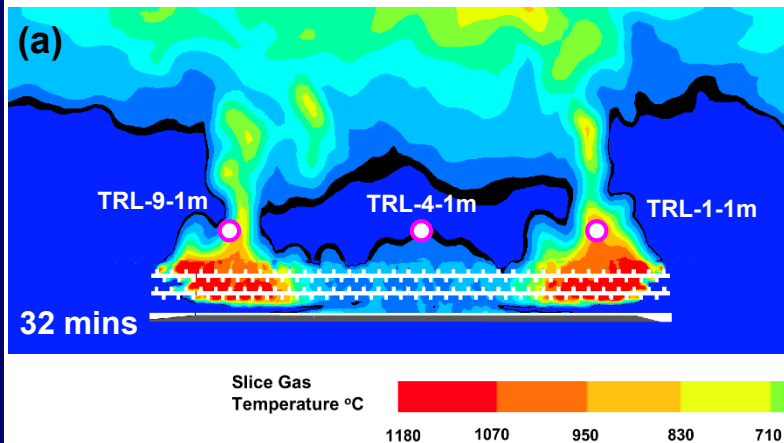
Comparison of thermocouple temperatures at compartment centreline along fire trajectory, TRL-4 to TRL-8, (a) ceiling level (note: TRL-5-2.7m failed during test data acquisition), (b) 2 m from floor level, (c) 1.5 m from the floor level, and (d) 1 m from the floor level (i.e., 0.265 m from the fuel bed top level).



# Model Prediction vs. Test Results



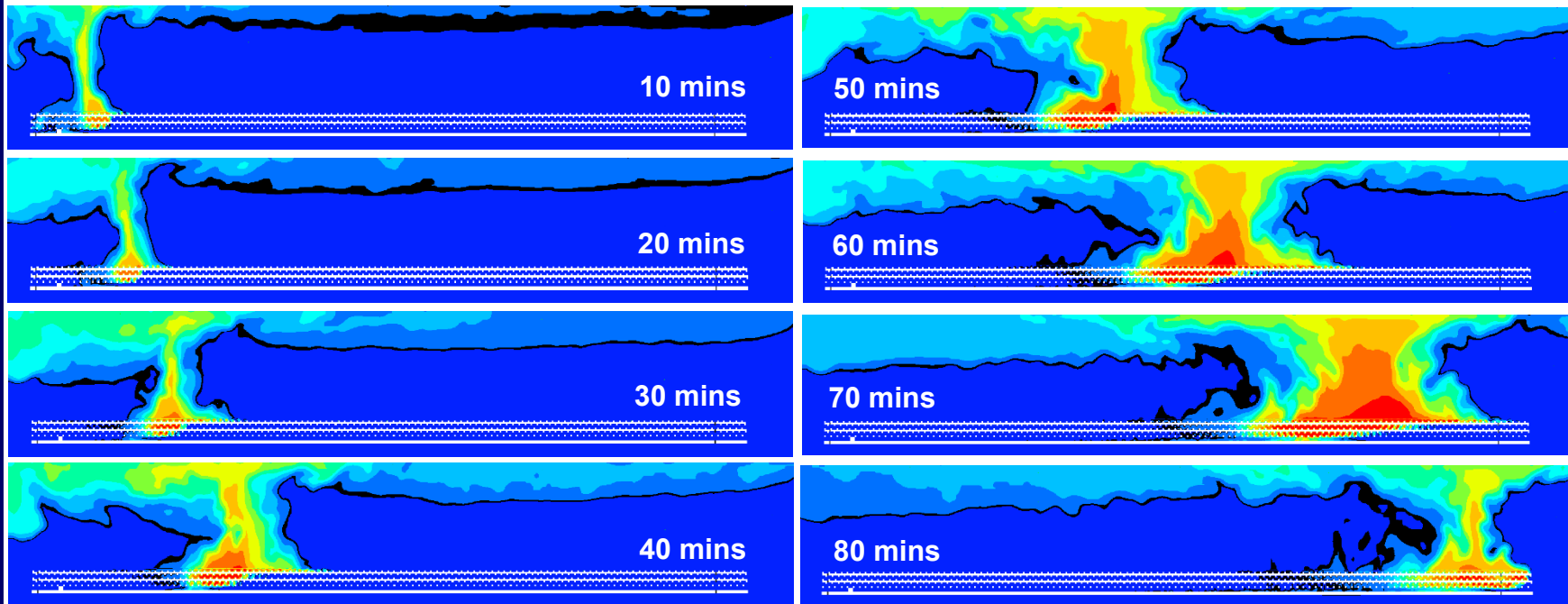
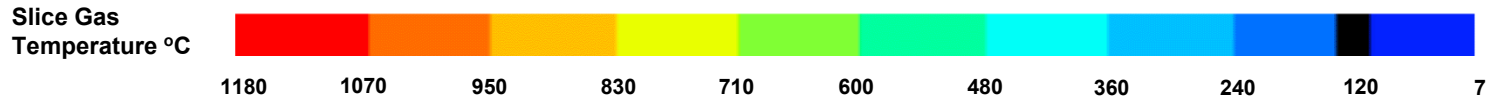
Comparison of thermocouple temperatures along fire trajectory and longitudinal fuel bed edges, (a) TRL-1 to TRL-3 at ceiling level, (b) TRL-1 to TRL-3 at 1 m from floor level (i.e., 0.265 m from fuel bed top level)



Gas phase temperature contour of the compartment 'slice' at specific time, (a) TRL-1/4/9 'slice' at 32 mins, (b) TRL-2/6/10 'slice' at 58 mins.

# Further Understanding on Test via Model in-depth Characterisation

## ○ Gas Temperature Contour

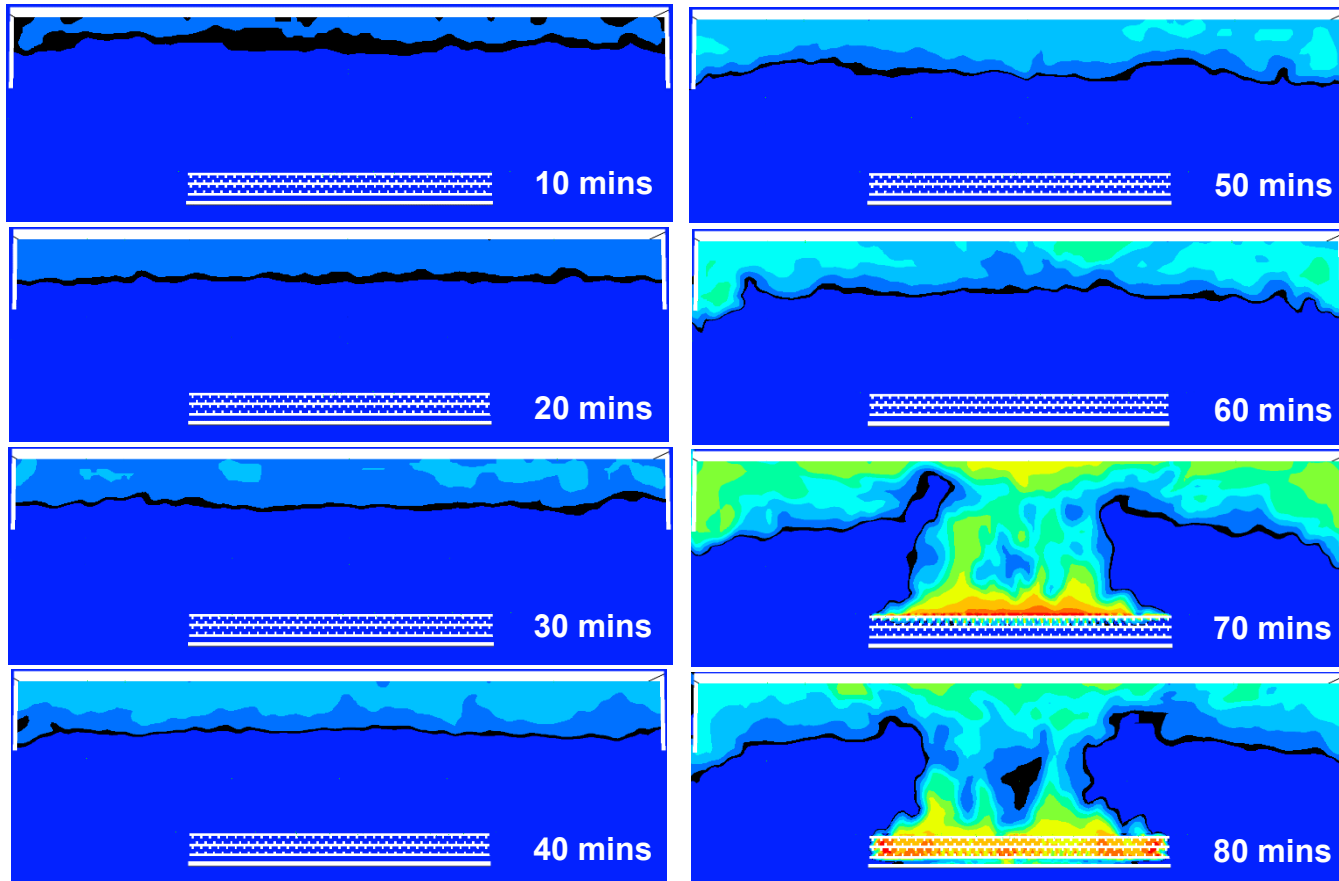
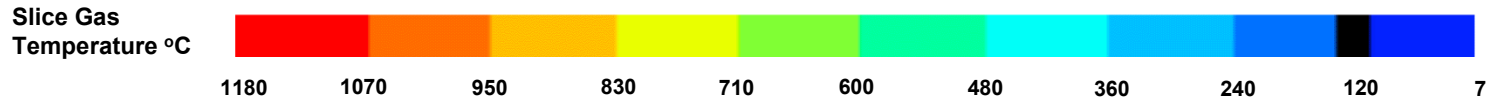


Gas phase temperature contour of the compartment central 'slice', wood sticks "obstruction" removed in Smokeview for clearer fire demonstration within the wood crib depth.



# Further Understanding on Test via Model in-depth Characterisation

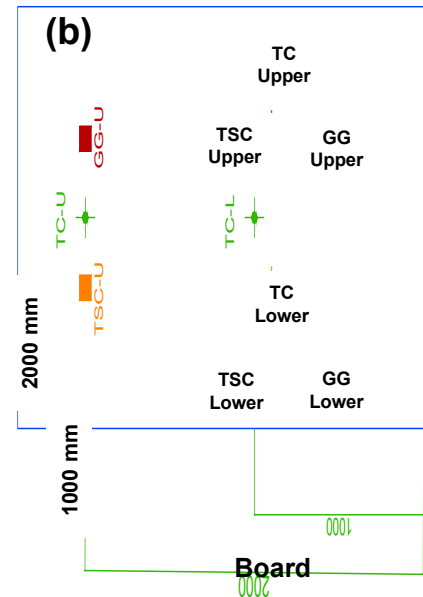
## ○ Gas Temperature Contour



Gas phase temperature contour of compartment far-field 'slice' (12.5 m from back wall) (wood stick "obstruction" removed in Smokeview for clearer fire demonstration within wood crib depth)



- **Incident Heat Flux**

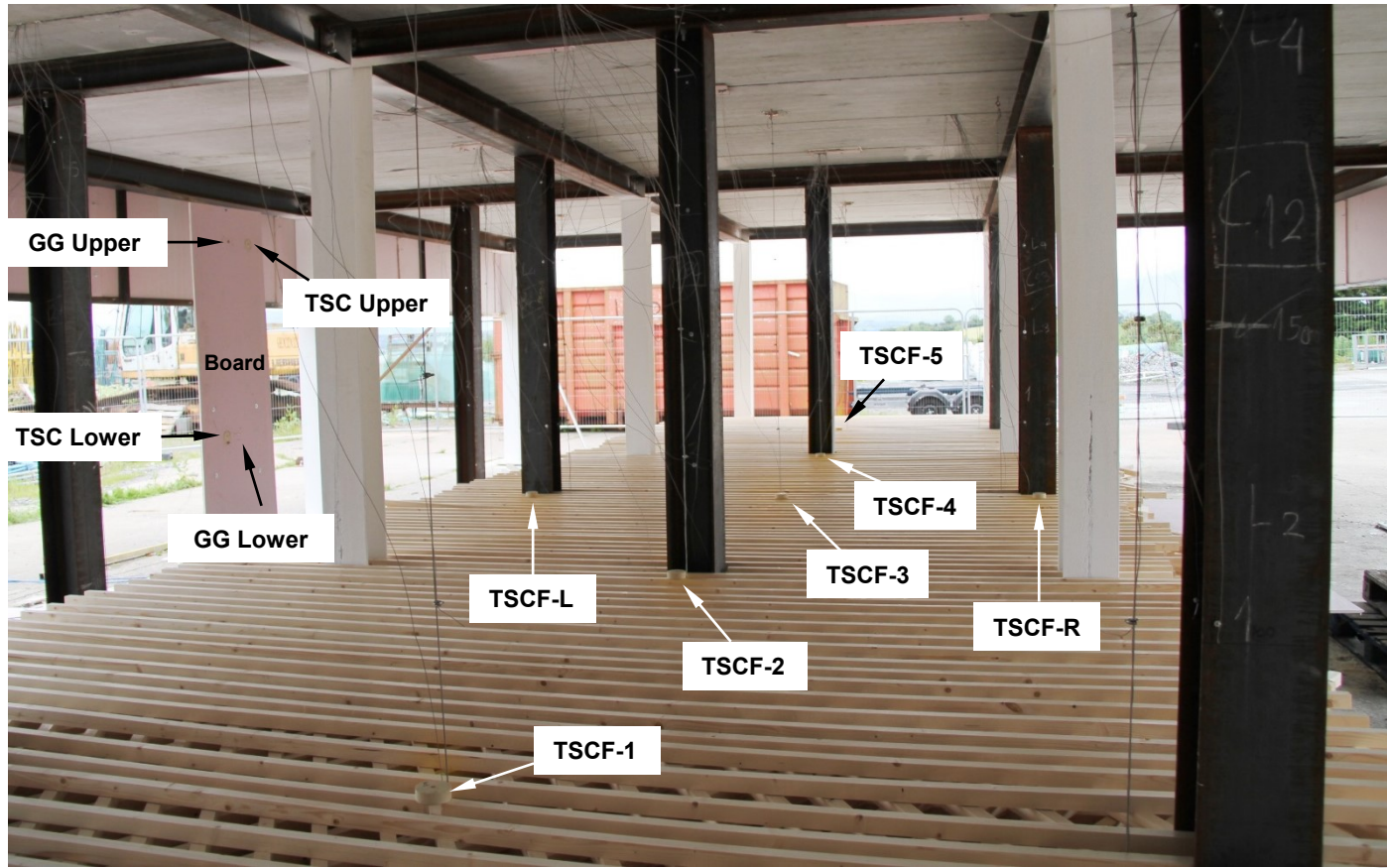


**Location of the heat fluxes instrumentations, (a) plan view, TSCF-1 to TSCF-5 were thin skin calorimeters (TSC) on top of the fuel bed level, (b) board in elevation view, instrumented TSCs, Gordon Gauges (GG), and thermocouples (TC).**

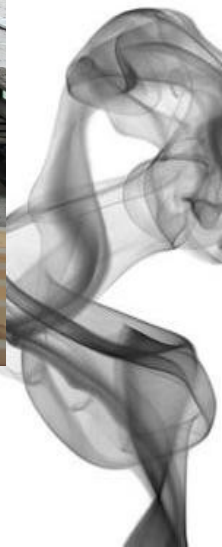


# Model Prediction vs. Test Results

## ○ Incident Heat Flux

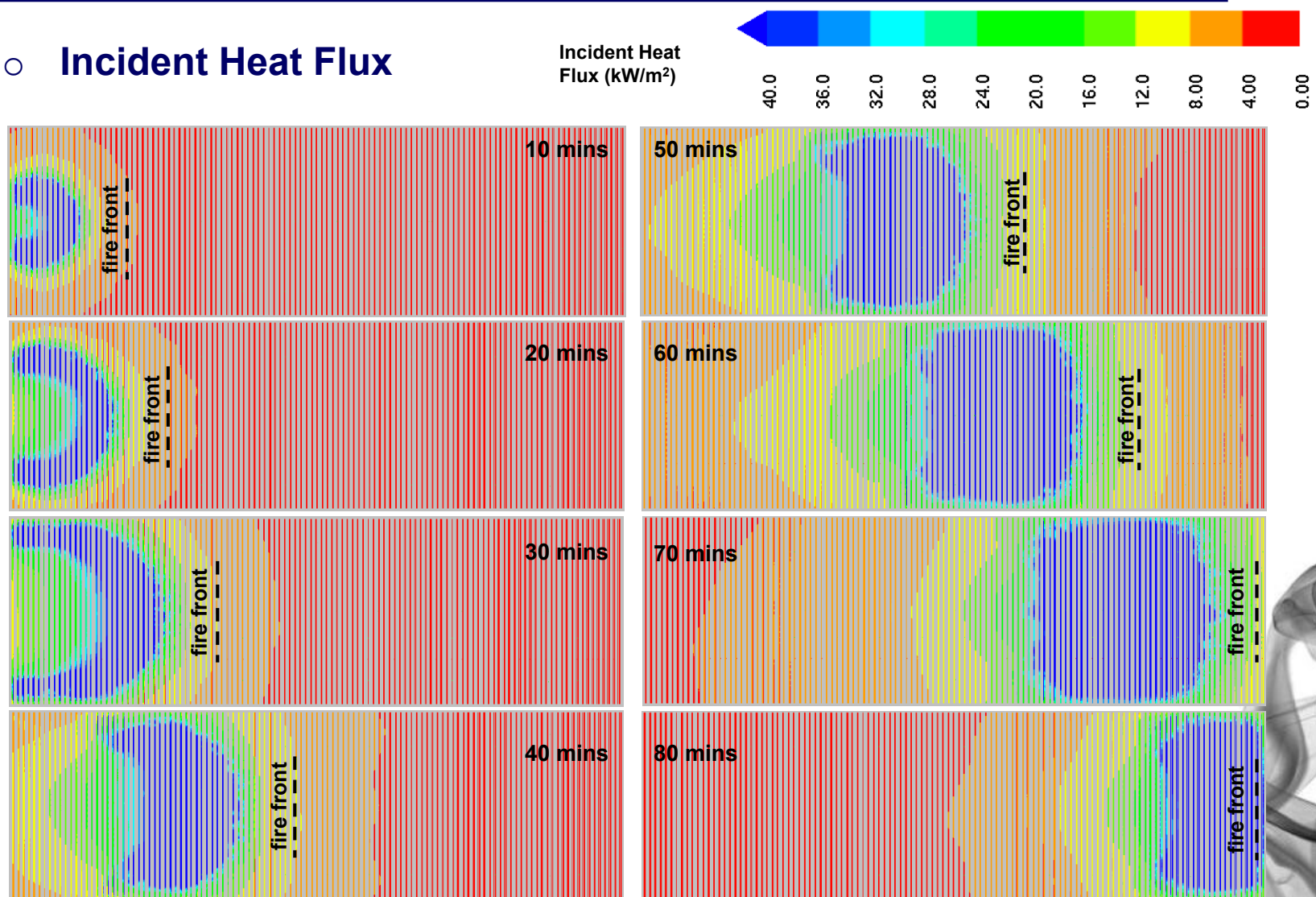


Location of the thin skin calorimeters (TSC) and Gordon Gauges (GG) inside of the compartment.



# Further Understanding on Test via Model in-depth Characterisation

## ○ Incident Heat Flux



Incident heat flux on the top layer of wood sticks with 10 mins intervals

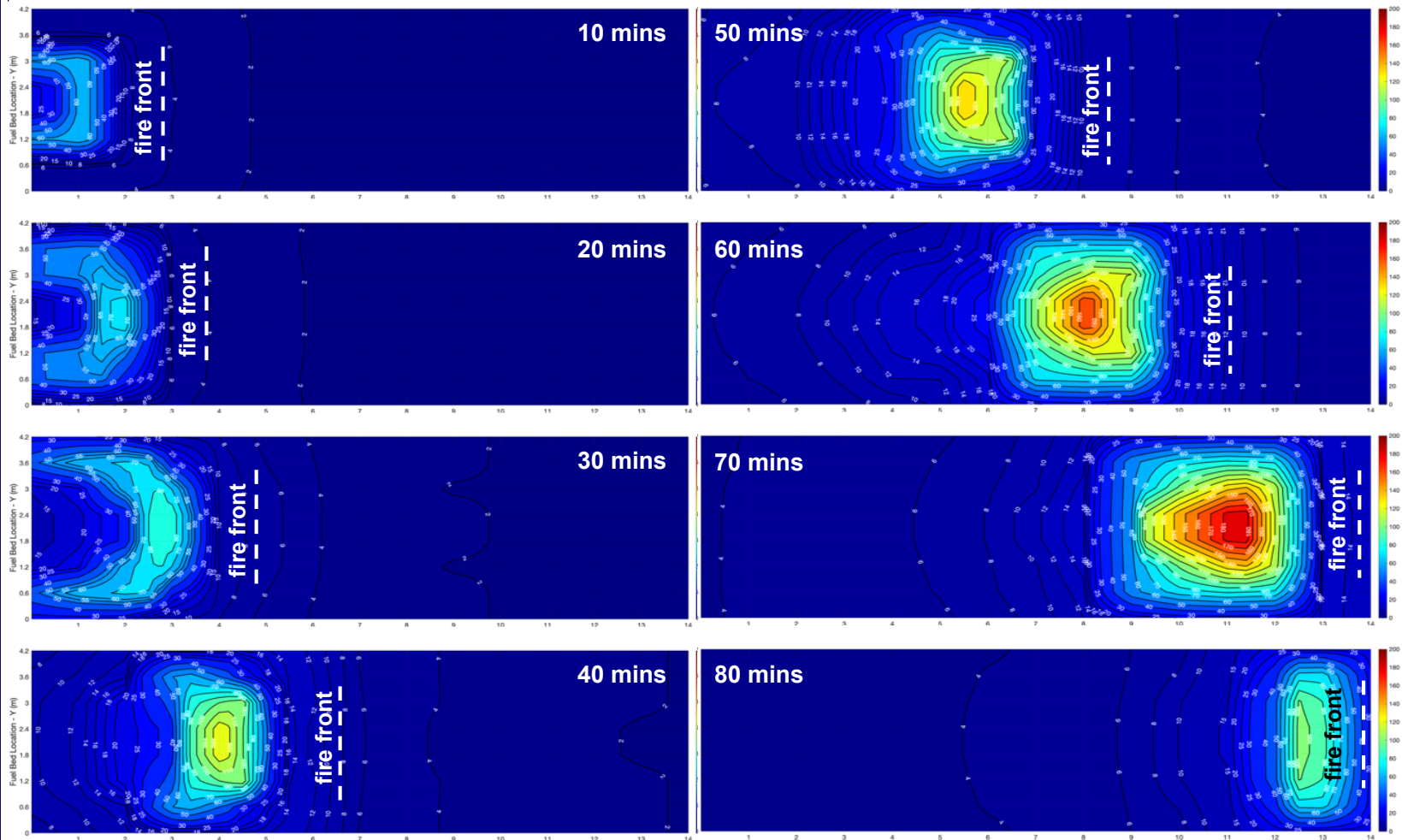
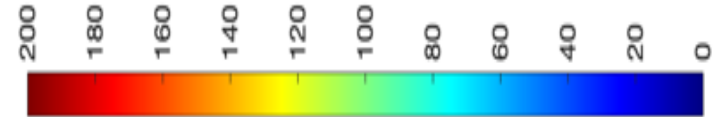




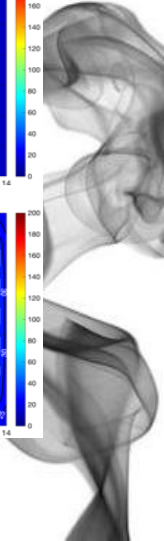
# Further Understanding on Test via Model in-depth Characterisation

## ○ Incident Heat Flux

Incident Heat  
Flux ( $\text{kW/m}^2$ )

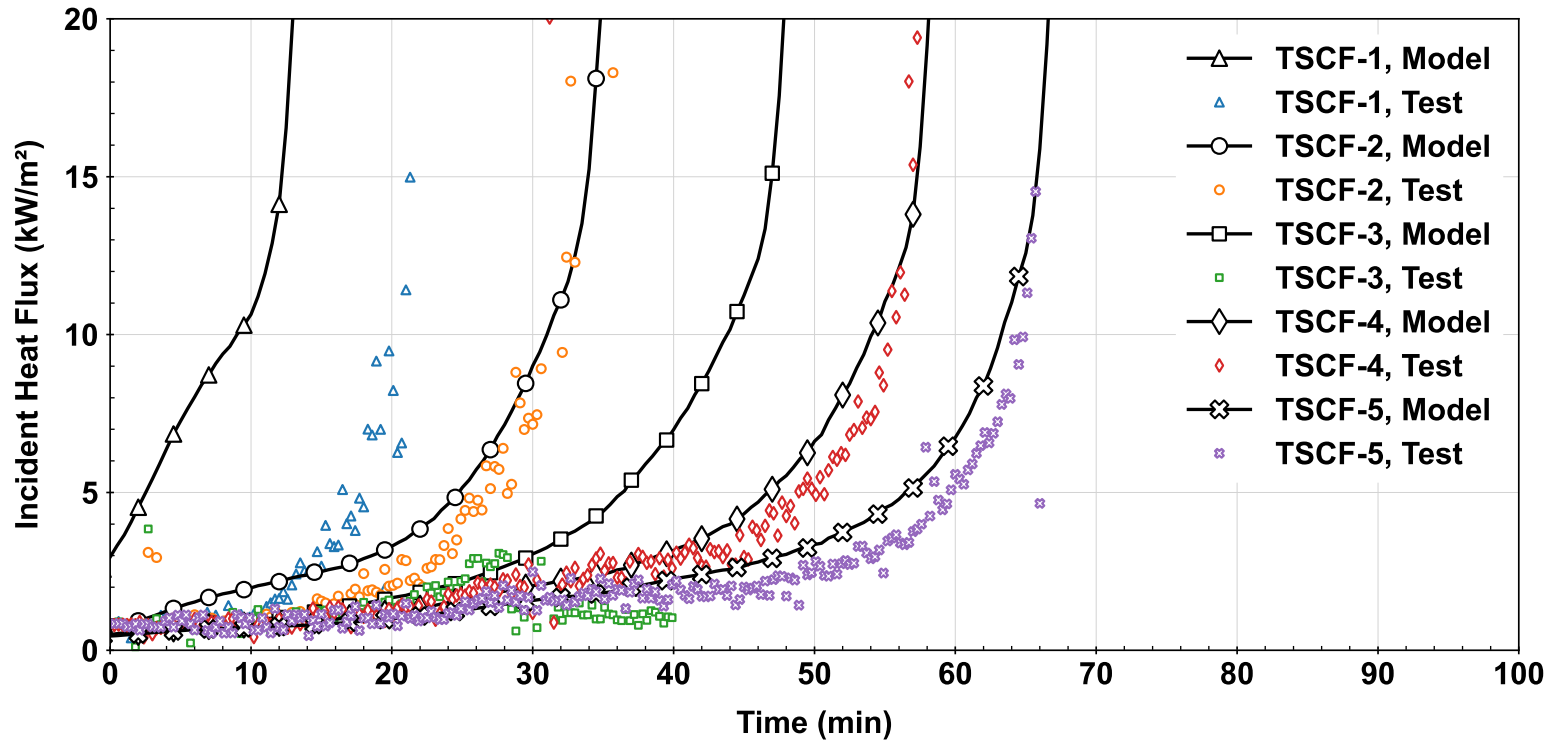


Incident heat flux on the top layer of wood sticks with 10 mins intervals

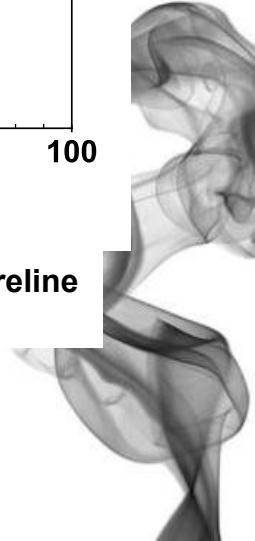


# Model Prediction vs. Test Results

## ○ Incident Heat Flux from TSC

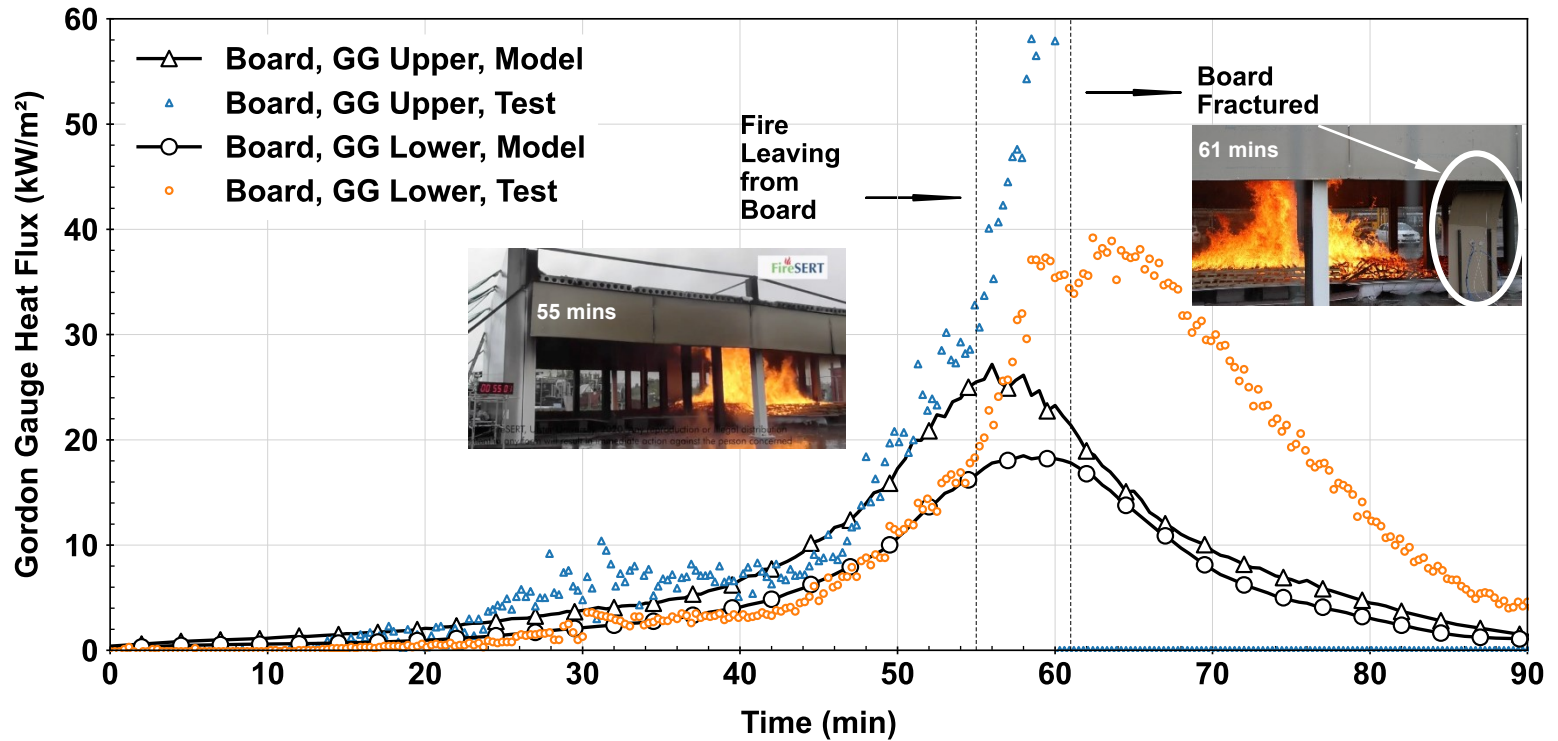


Comparison on incident heat fluxes from thin skin calorimeters (TSC) at fuel bed top level centreline along fire trajectory (TSCF-3 failed during test data acquisition after 30 mins).



# Model Prediction vs. Test Results

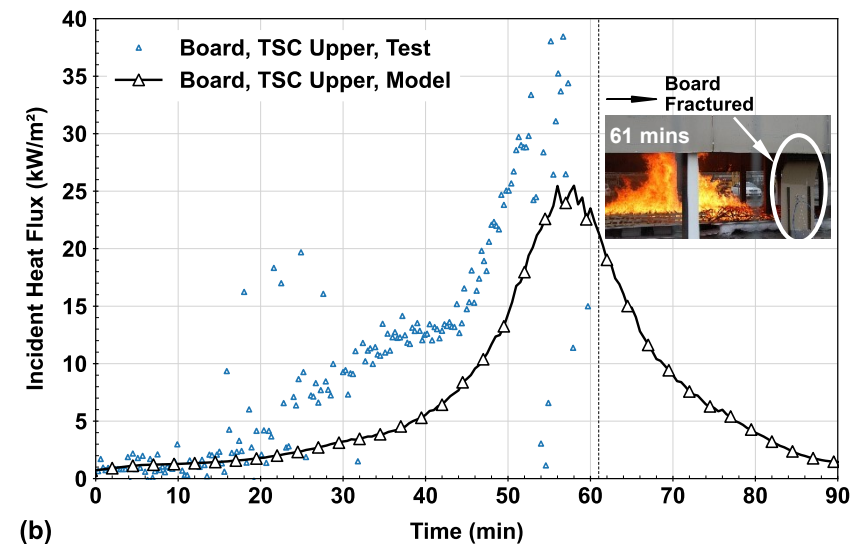
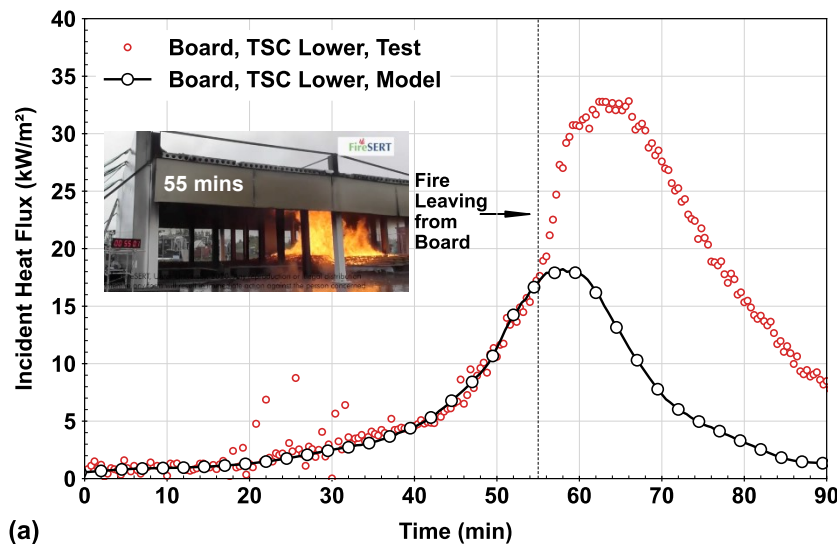
## Heat Flux from Gardon Gauge



Comparison between the test and the model on Gardon Gauges (GG) measured heat fluxes (GG Upper failed due to board fracture at 61 mins).

# Model Prediction vs. Test Results

## Incident Heat Flux from Thin Skin Calorimeter (TSC)



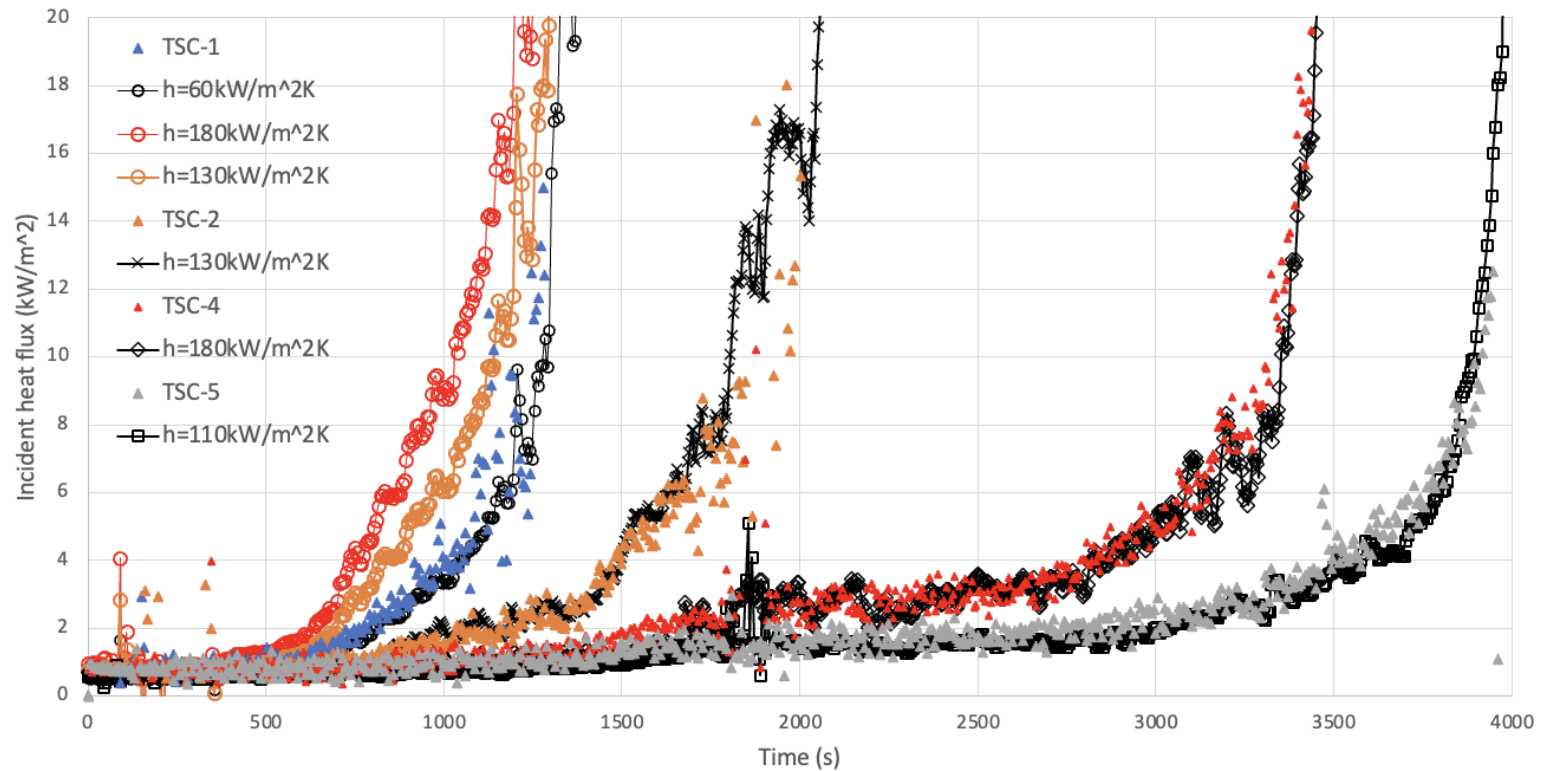
Comparison on incident heat fluxes from thin skin calorimeters (TSC) on the board, (a) TSC Lower, and (b) TSC Upper, (failed due to board fracture at 61 mins).



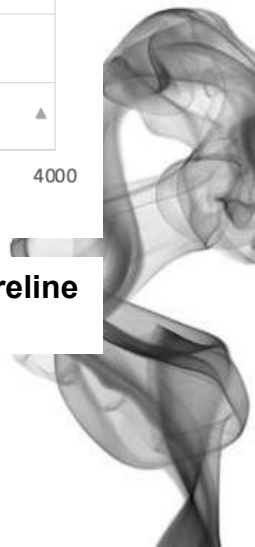


# Model Prediction vs. Test Results

## ○ Incident Heat Flux from TSC



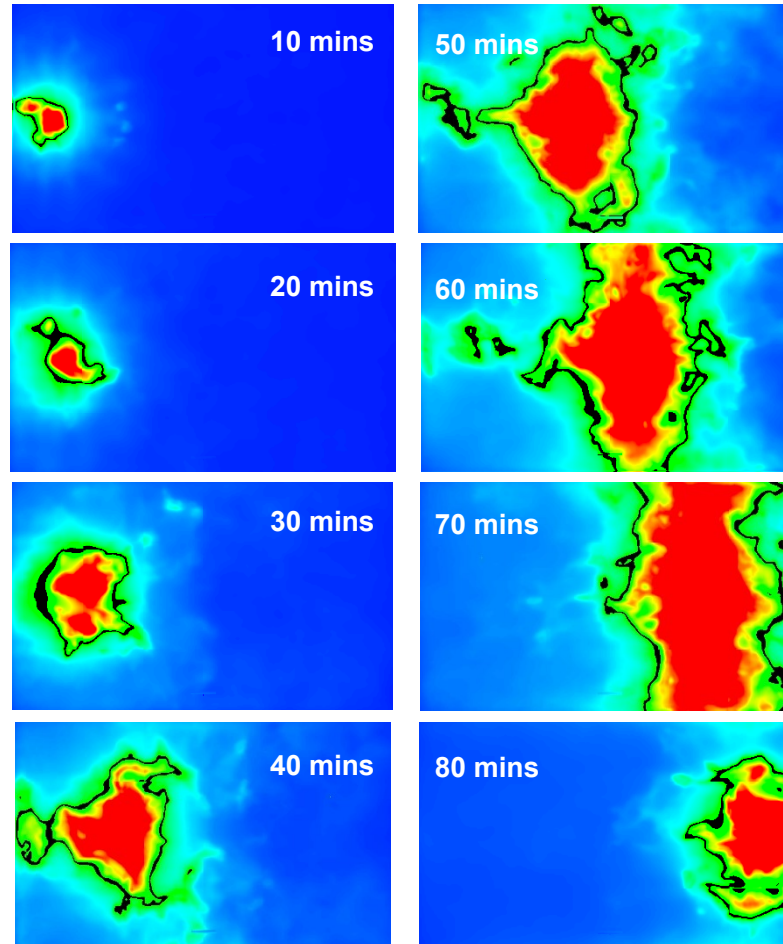
Comparison on incident heat fluxes from thin skin calorimeters (TSC) at fuel bed top level centreline along fire trajectory (TSCF-3 failed during test data acquisition after 30 mins).



# Further Understanding on Test via Model in-depth Characterisation

## ○ Incident Heat Flux

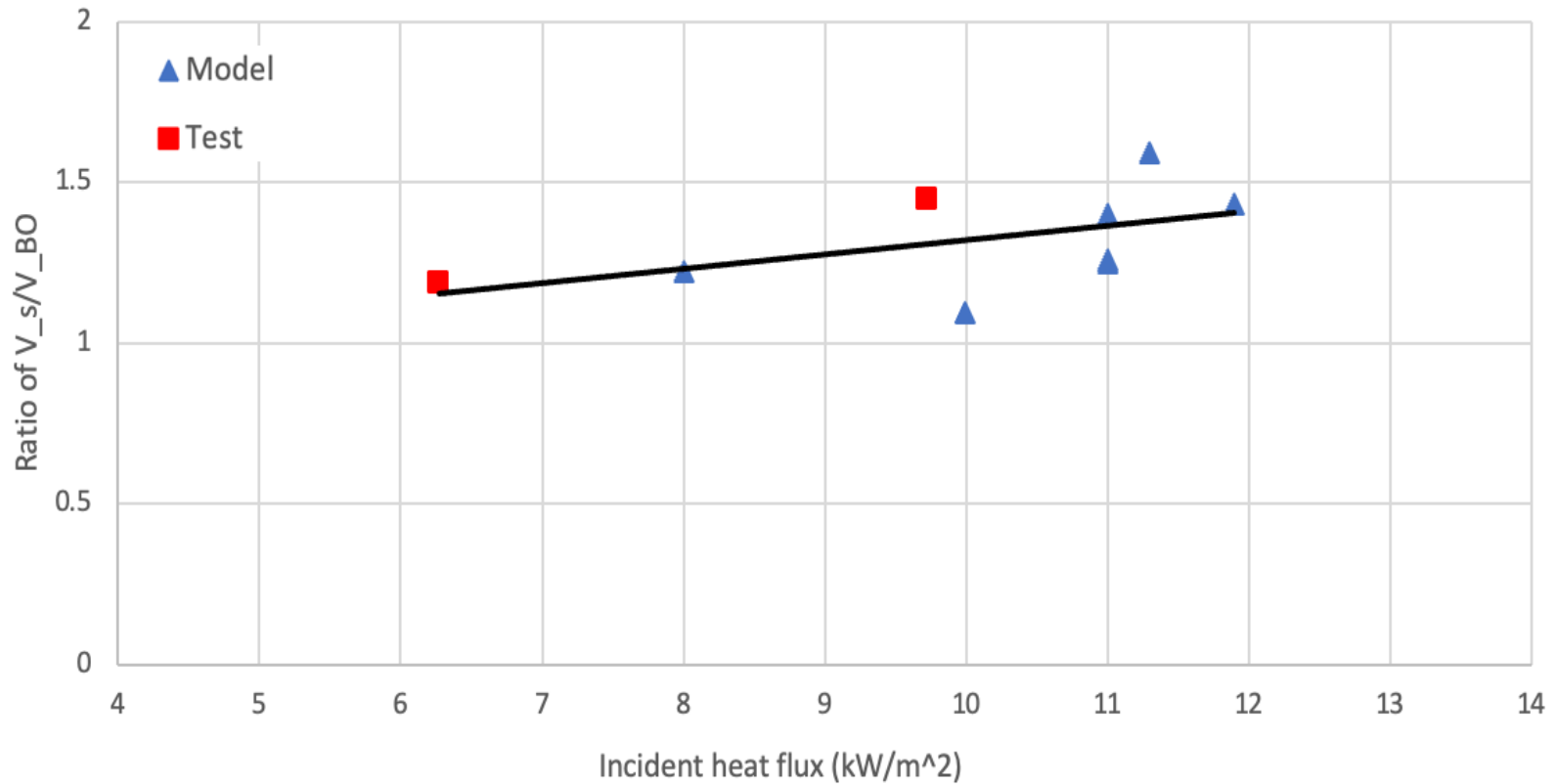
Incident Heat  
Flux ( $\text{kW/m}^2$ )



Incident heat flux on compartment ceiling with 10 mins intervals



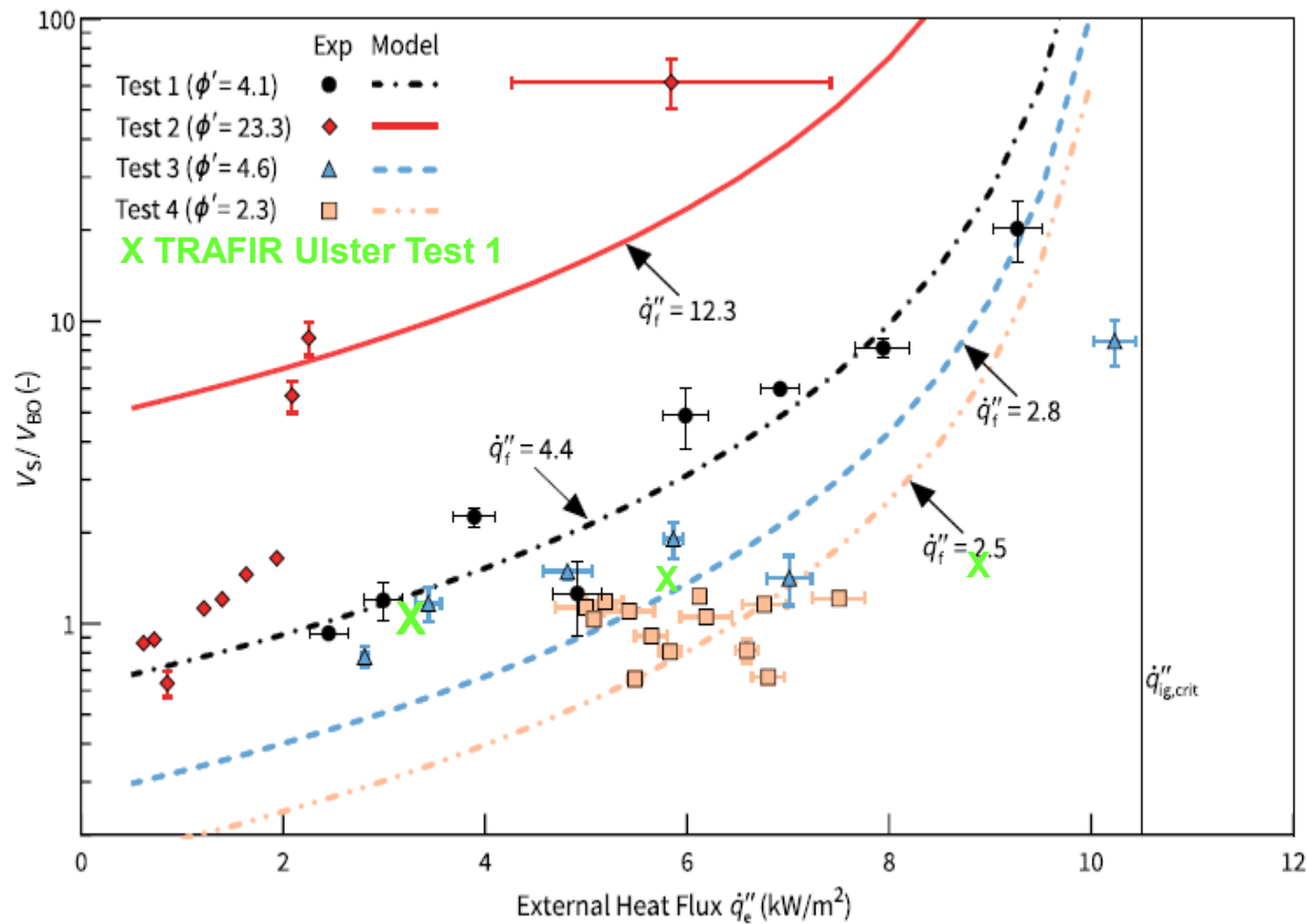
# Further Understanding on Test via Model in-depth Characterisation



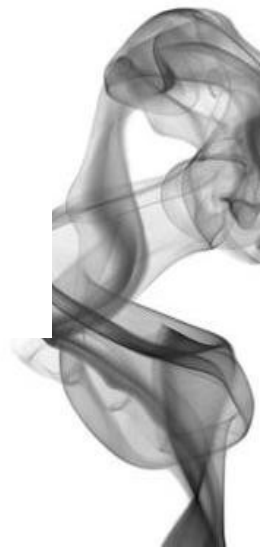
Linear regression of  $V_s/V_{BO}$  against the incident heat flux  
(for Test 1 with inverse opening factor = 3.6)



# Phenomenological model compared to experimental data

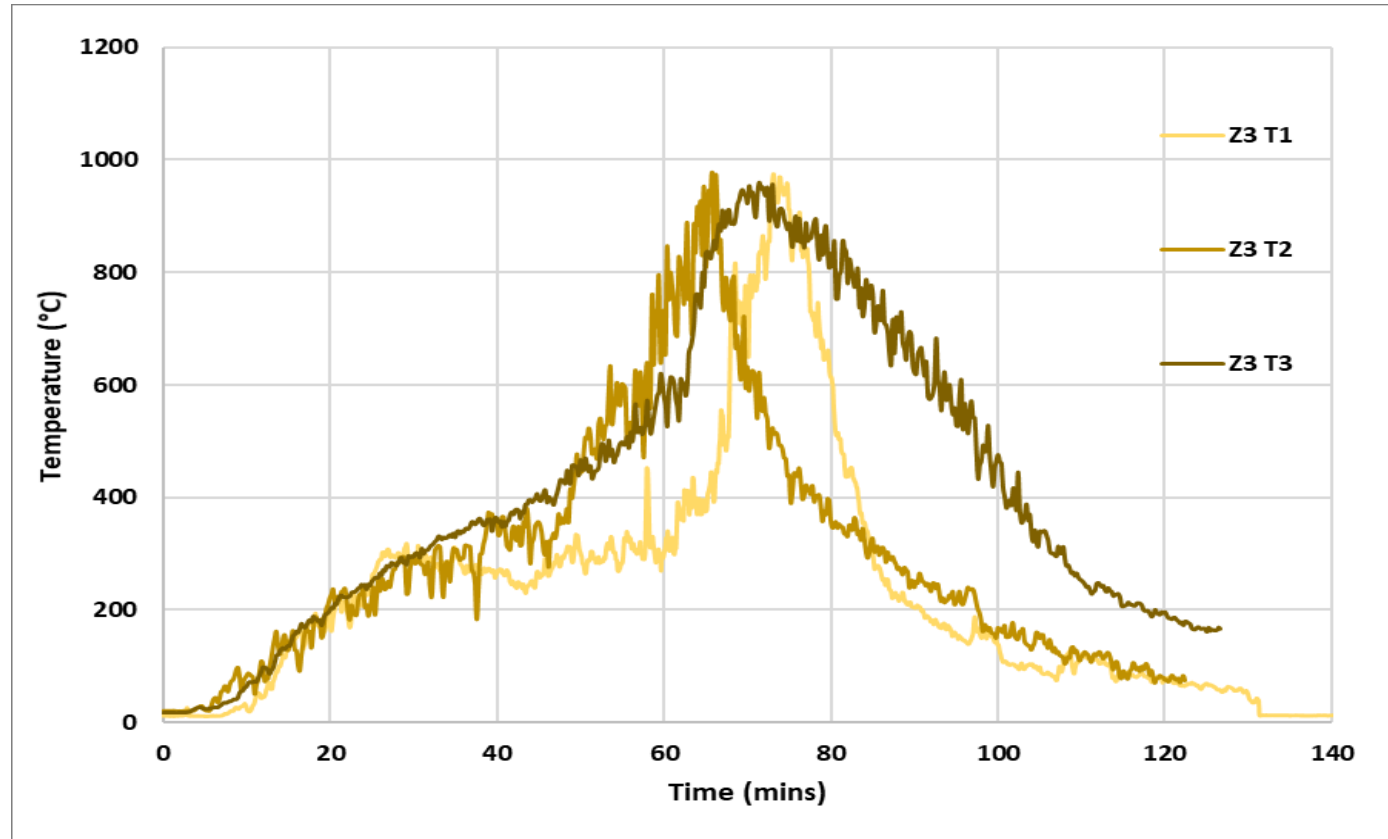


Gupta, V, Osorio, AF, Torero, JL, & Hidalgo, JP 2021, 'Mechanisms of flame spread and burnout in large enclosure fires', Proc. Comb. Inst. 38(3):4525–4533





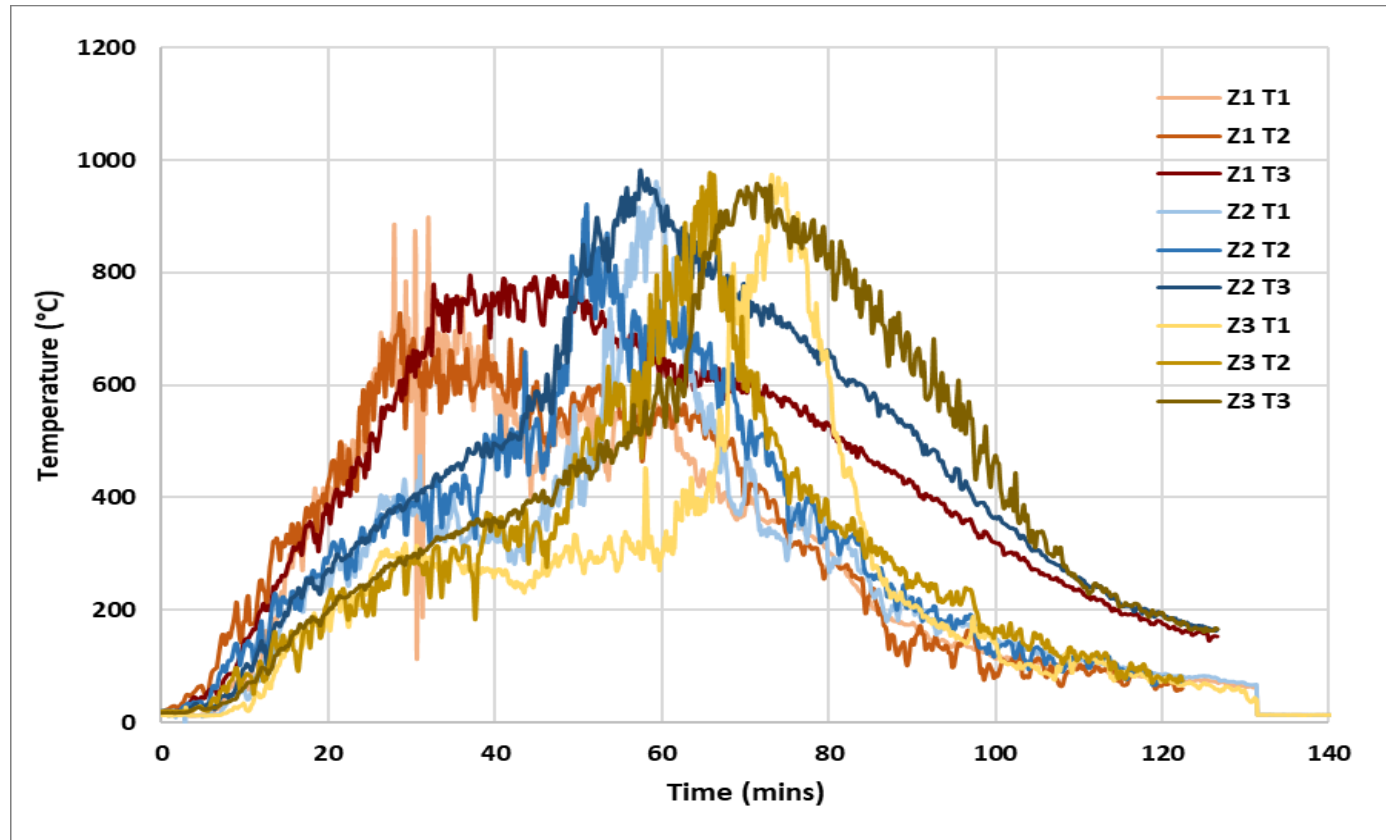
## Opening factor study – test comparison (T1-3)



Temperature history at top of compartment in third bay – Test 1-3



## Opening factor study – test comparison (T1-3)

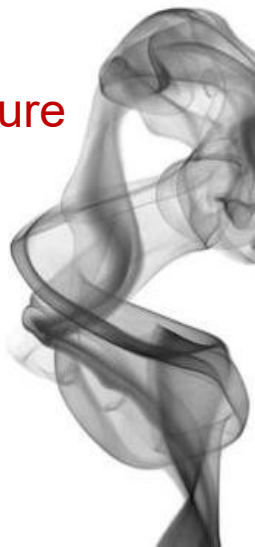


Temperature history at top of compartment in third bay – Test 1-3



# Conclusions (1)

- Reconstruction of a uniform wood fuel bed for fire spread, is achieved through using a **stick-to-stick model with simple pyrolysis** and an ignition temperature setup. Compared with previous research the results show more parameters being comparable to the full suite of test data, suggesting potential credibility of the model for predicting **fire spread rate, flame temperature, incidental radiant heat flux, burn away, and most importantly, the total HRR evolution.**
- Previously observed **discrepancies in the cooling phase temperatures are predominantly associated with limitations in representation of heat transfer processes associated with the glowing char; explicit treatment not currently included in FDS.**
- The mesh scheme which adopts a **finer mesh within the crib structure and relatively coarse mesh in the gas phase**, provides a viable practical solution for modelling such crib fires, with potential for scaling up to compartment level. Some differences are found but they may be expected to be small when spread on upper surface of crib driven mainly by remote heating, not local flame front.



## Conclusions (2)

- Results with a very fine mesh inside the crib structure (now 7.5/8.75mm cells, giving 12x4 cells between sticks in elevation) have **confirmed the plausibility of the original results with a coarser mesh** (15/17.5mm cells with 6x2 cells between sticks).
- The single crib baseline model has a total of 1.3M cells, simulation of 20 minutes test using 16 processors requires ~4 x 48hr jobs; **the fine mesh models run ~14 times as slowly**, hence main parametric study done with baseline model (~10 parameters, x3 cases each = 30 simulations, as reported previously).
- The “scaled-up” model has a total of 8.3M cells, simulation of 72 minutes test using 125 processors requires ~40 x 48hr jobs on ARCHER2 (x 6 parametric variants = ~10,000 CU); hence the running speed per cell per processor per minute test time **is 30% of that for the single crib**, mainly due to greater complexity of the fire.



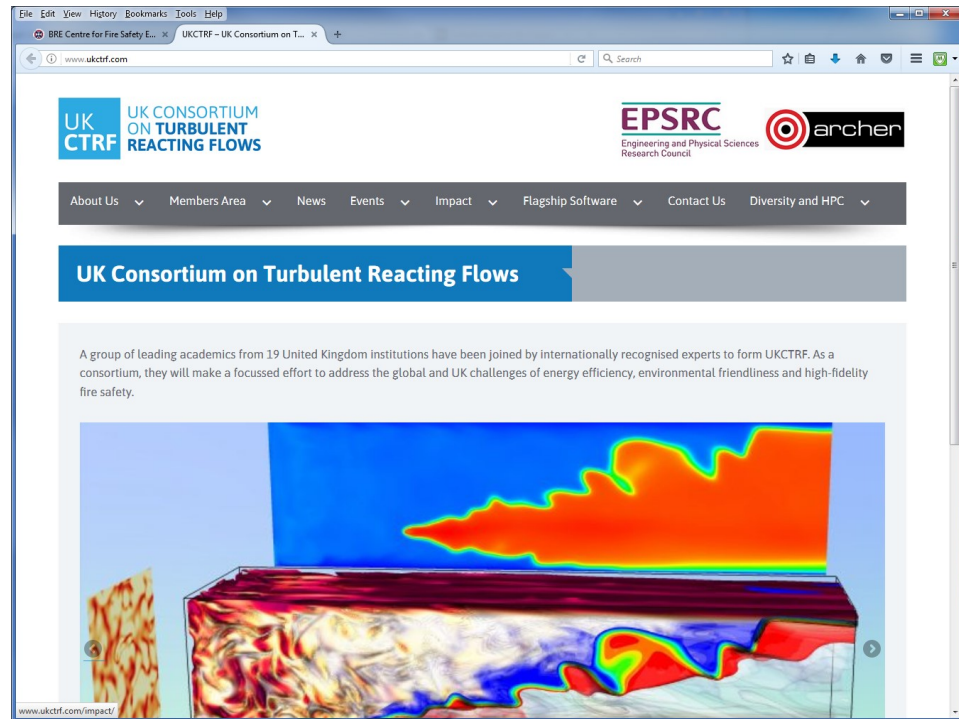


## Conclusions (3)

- A scaled-up stick-by-stick CFD model for fire spread within the large compartment of 15.2m x 9.2m x 2.8m, again demonstrates **a promising capability in predicting the evolution of fire spread and burn-away** as well as in reproducing main features of gas phase temperatures along the fire travelling trajectory; nevertheless there are some differences in peak temperatures which arise from details in shape of simulated fire plume and again major differences in the cooling phase.
- The potential for this approach to reproduce **different fire conditions with more restricted ventilation** (inverse opening factors 3.2, 13.7 & 41.7) is now being assessed via comparisons with TRAFIR Ulster Travelling Fire series (x3), to explore method generalisation potential/compare with phenomenological/theoretical models in terms of fuel bed heat fluxes
- When further validated, this CFD method will provide a capability for **numerical “fire experiments” for exploring structural response to variations in the design parameters** (e.g., ventilation conditions, fuel arrangement, ceiling height, etc.), which are generally out of reach via conventional large-scale structural fire tests under travelling fires.



# Acknowledgements (1)



**EPSRC EP/R029369/1: Addressing Challenges Through Effective Utilisation of High Performance Computing – a case for the UK Consortium on Turbulent Reacting Flows (UKCTRF)**

<https://gow.epsrc.ukri.org/NGBOViewGrant.aspx?GrantRef=EP/R029369/1>



# Acknowledgements (2)

## Fire degree project students

**Structural and Fire Safety Engineering Dissertation (90 credits)**  
**MEng thesis (50 credits)**

### 19/20 students

- **Chang Liu (SAFE), Yang Xu (SAFE)**



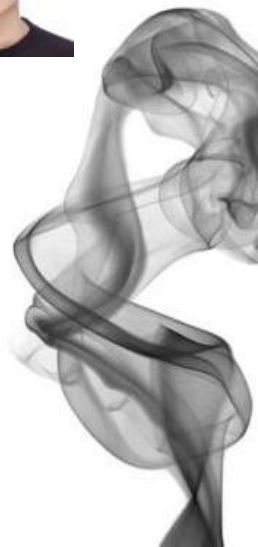
### 20/21 students

- **Peter Charley (MEng), Chang A. Liu (SAFE)**

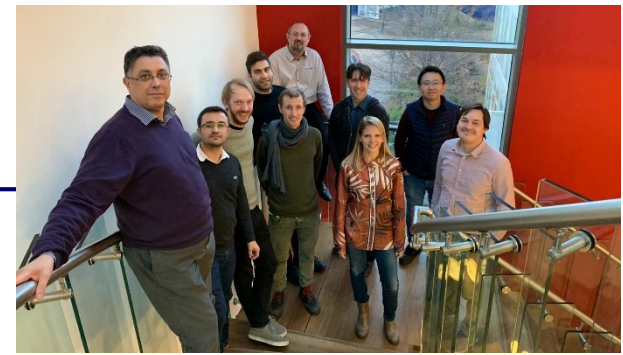


### 21/22 students

- **Weitian Lu (SAFE), Yanchi Mo (SAFE)**



# Acknowledgments (3)



## TRAFIR Project

Characterization of **TRA**velling **FIRE**s in large compartments

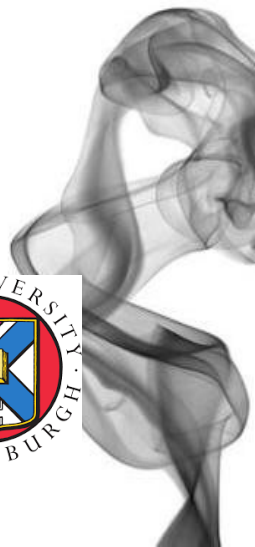
Funding from the Research Fund for Coal and Steel (RFCS) - European Commission

Industrial led – ArcelorMittal  
(1/07/2017 → 31/12/2020)



- **testing** (isolated elements and simplified fire progression, as well as a full-scale large compartment)
- **modelling** (both simplified analytical/phenomenological models and CFD).

Project partners:





# Edinburgh fire

- **Colleagues and students:**
  - 7 Academic Staff (+1 retired)**
  - 5 Research staff**
  - c. 20 PhD Students**
  - 25+ MSc students**
  - ~10 pa UG students**
  - Visiting researchers**
- **External Relationships:**
  - **EPSRC**
  - **ArcelorMittal (RFCS TRAFIR project)**
  - **BRE Trust (FireGrid, PhD Intelligent Egress)**
  - **Fire & Rescue Services**
  - **International academic/research partn**
    - **UQ (Hidalgo, Maluk, Lange, Gupta...)**
    - **CVUT Prague (Wald, Horová...)**
    - **RISE (Sjöström, ...)**
    - **Liège (Franssen, Gamba...)**
    - **Ulster (Nadjai, Alam...)**



# Questions?

